

technical bulletin

NATIONAL COUNCIL OF THE PAPER INDUSTRY FOR AIR AND STREAM IMPROVEMENT, INC., 260 MADISON AVENUE, NEW YORK, N.Y. 1001

A REVIEW OF VARIABILITY IN EFFLUENT QUALITY DISCHARGED BY SELECTED PULP AND PAPER INDUSTRY SOURCES

TECHNICAL BULLETIN NO. 355

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Selection of the appropriate relationship between the annual average, maximum 30 day, or maximum daily effluent quality limitations for BOD and total suspended solids is of particular interest to the pulp and paper industry, since these values are commonly incorporated into discharge permits. The subject was addressed extensively by the National Council staff in the development of existing effluent guidelines, and continues to be an important element of the technical studies program.

The attached technical bulletin is a review of the methods used by EPA, and described in the Development Document for the Phase III Effluent Guidelines. The review was carried out at the Northeast Regional Center under the direction of James J. McKeown, Regional Manager. The technical bulletin was prepared by David B. Buckely, Research Engineer, who has assisted in statistical program development by Dr. Linfield C. Brown, Tufts University, Department of Civil Engineering, and Karl T. Dussick, NCASI computer programmer. This portion of the study served as the basis for comments on the variability issue to EPA on the Phase III effluent guidelines new source performance standards. Additional studies are currently underway which will provide a basis for further comments to EPA on the variability issue.

The bulletin contents include a review and description of the methodology used by EPA to arrive at maximum 30 day and maximum daily limits, as well as alternate methods used by the Council staff. The data base draws upon a 33 mill "verification phase" data base common in part with that used by EPA but excluding a significant number in this total group of about 55 where the data were judged for one or more reasons to be inadequate for use in this study. It also draws upon, and uses extensively information in the Council's continuing treatment plant performance data collection program from 34 mills. In total about 75 years of data were examined. The study suggested several modifications in the EPA methodology for developing maximum day and maximum 30 day averages which would more nearly reflect the variability in treatment plant performance for BOD and total suspended solids over the life span of permits. Among these were, (a) a change in the percentile selected for use in non-parametric statistical analysis, (b) the use of additional test procedures for goodness of fit, (c) statistical distributions capable of more nearly characterizing performance over the five year permit span from one year of data or a more extensive data base, and (d) the development of variability factors reflecting a probability of occurrence.

Your comments and questions on the contents of this technical bulletin are solicited and should be directed to this office or to Mr. McKeown or to Mr. Buckley at the Northeast Regional Center.

Yours very truly,

Russell O. Blosser Technical Director

ROB:mm Attach.

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A REVIEW OF VARIABILITY IN EFFLUENT QUALITY DISCHARGED BY SELECTED PULP AND PAPER INDUSTRY SOURCES

I INTRODUCTION

A. Background

Characterizing the variation in effluent quality from pulp and paper industry treatment systems has been a major activity in the development of effluent limitations. The publication of EPA's Development Document (1) in December 1980 represents a fourth attempt in assessing the varying nature of two wastewater constituents, biochemical oxygen demand (BOD₅) and total suspended solids (TSS). The initial effort occurred with the use of "interim" guidelines in the processing of discharge permits under the Refuse Act Permit Program while the second and third examinations of variability were developed during the Phase I and Phase II assessment of best practicable treatment (BPT) technology for the industry.

The Development Document (pp. 442-451) contains the methodology used in assembling and analyzing the treatment system performance data which provided the basis for the variability factors proposed for use in the Phase III Effluent Guidelines, Best Conventional Treatment (BCT) Options 1 and 4. These factors are being proposed for regulating effluent quality for all paper industry production categories although some difference in variability is being proposed for the nonintegrated tissue, lightweight, filter and nonwoven, and paperboard categories.

The variability referred to in the Development Document is the relationship of two periods of treatment system discharge quality to long-term performance; specifically, the ratio of maximum daily (MD) effluent quality to annual (or long-term) average (AA) performance and the ratio of the maximum thirty consecutive day (MA30CD) performance to the annual average. Inherent in the examination of these two periods of treatment system performance is the relationship of a third variability period, the ratio of the maximum daily (MD) discharge to the maximum thirty consecutive day (MA30CD) effluent Table Al contains the variability used in previous BPT quality. effluent limitations and those proposed for BCT technology. Table A2 represents the effluent quality specified for BPT and proposed BCT technology. (Note: These Tables are contained in the Appendix.)

B. EPA Data Base

To adequately comment on the appropriateness of the variability proposed for BCT technology, the performance data used in the variability analysis were obtained from the E.C. Jordan Company in IBM-Diskette form. The data were adapted for analysis at the NCASI Northeast Regional Center which uses a DEC-10 data processor and are referred to as "verification mill" data. Subsequent effort was required to properly identify the waste streams provided and the production category to which the data pertained. The treatment system data were identified by "308" numbers and no treatment process description was provided; however, additional information received by NCASI from the EPA public record (2) allowed a general description of the treatment processes used at each mill. Fiftyfour mills are represented in this data base and production categories are classified as singular; i.e., no crossovers in production existed at these locations. Approximately 11-13 months of data were provided by each of the mills.

C. NCASI Data Base

To supplement the EPA data base, the National Council's treatment system performance program was reviewed for categorical pure mill candidates. Forty-two mill locations were initially selected for variability analysis. The extent of data provided by these mills ranged from nine months up to five years, although most of the data analyzed represented twelve months of performance. Multiple years of data, when available, were divided into increments of approximately twelve months to provide a time frame comparable to that used in the EPA variability analysis.

Table A3 contains the mills initially reviewed for variability analysis. Also indicated is the treatment process used at each mill and the time frame of the data provided by the individual mills.

II. STATISTICAL TECHNIQUES USED IN CHARACTERIZING VARIABILITY

A. EPA Approach

The Development Document contains two approaches to the estimation of the variability factors proposed for BCT effluent limitations. One technique is a nonparametric method used to estimate the maximum daily effluent quality. The other technique utilizes a "quasiparametric" method for estimating the maximum thirty consecutive day discharge. These values divided by the long-term average discharge for the particular parameter (BOD₅ or TSS) result in MD and MA30CD variability factors. Both methods will be briefly discussed in the following.

(1) <u>Maximum Daily Variability Factor</u> - Initially, EPA examined the BOD₅ and TSS daily discharges to determine if the data conformed to classical statistical distributions such as the normal or log-normal distribution. If the data fit such a distribution, then a parametric method could be used to estimate a maximum daily discharge. The Kolmogorov-Smirnov goodness-of-fit test (see Reference 3) was used to test the data to see if the daily data could be described by a normal or log-normal distribution. The Development Document cited that "in general, neither the normal nor log-normal distribution adequately represent the mill specific daily pollutant discharge value of BOD₅ and TSS." Analysis (2) supportive of this observation, however, did indicate that some 26 and 28 mill treatment systems did adhere to either the normal or log-normal distribution for daily BOD₅ and TSS discharges, respectively. The log-normal distribution predominated in the characterization of the individual mill discharges. Because the mill discharges did not completely adhere to one or the other distributions, EPA selected a nonparametric method.

The nonparametric method is a ranking technique where the daily discharges are assembled in order of magnitude. A specific percentile is selected along with a tolerance level (or confidence level) at the chosen percentile. The tolerance level indicates the degree of confidence surrounding the percentile. EPA utilized the 99th percentile at the 50 percent tolerance level in estimating the maximum daily discharges. It is not clear in the Development Document why the 99th percentile was chosen as this estimate produces a probability that 3 to 4 occurrences may exceed the 99th percentile in a year's time. In addition, why a lower tolerance level (i.e., a higher degree of confidence surrounding the estimate) was not selected is not specified in the Development Document. This oversight is particularly puzzling because the maximum daily discharges are really not-to-exceed levels. The 50 percent tolerance level at the 99th percentile indicates that there is a 50 percent probability that the 99th percentile is higher than the value selected. If, for example, a 5 percent tolerance level (or 95% confidence limit) were used, the degree of confidence surrounding the estimate of the 99th percentile would be increased. In other words, there would only be a 5 percent chance of making the wrong estimate for the 99th percentile rather than a 50 percent chance. Nonparametric methods are described in <u>References 4</u> and 5; and the use of this technique will be demonstrated later in this report. In summary, the proposed maximum day variability factors for the discharge of BOD5 and TSS have been estimated by EPA with the following method:

Maximum Day Variability Factor = 99th Percentile @ the 50% Level Long-Term Average

(2) <u>Maximum Thirty Day Variability Factor</u> - The method employed by EPA in developing the thirty day maximum variability factors was cited earlier as being "quasi" parametric in that it does utilize standard parametric methods. However, it can also be considered nonparametric in that no assumption is made concerning the distribution of the population (in this case the daily BOD₅ and TSS discharge data) from which the thirty day means are drawn. The "quasi" parametric approach has its basis in a theorem known as the Central Limit Theorem. Stated loosely, the theorem says that the sum of a number of individual components, none of which dominate, tends to be a normal distribution as the number of components increases (3). For example, the cumulative annual effluent quality is being considered as the result of individual thirty day treatment system performances (or components) and according to the Central Limit Theorem, the individual thirty-day discharges would tend to be normally distributed around the mean of the thirty day values.

EPA assembled the individual daily discharge values into individual thirty consecutive value periods. If voids (missing data) existed in the daily data, the data record was "crunched" together to obtain the required thirty values. For example, if data were collected at a frequency of 15 observations per month, then a "crunched" thirty-day period could possibly extend over a sixty-day performance period. The impact of "crunching" the data on assessment of maximum thirty-day performance was not demonstrated. The individual thirty days of data at each mill were averaged and then subjected to a goodness-of-fit test (Lilliefors Test) to determine if the individual thirty successive days of data conformed to a normal distribution. When sufficient record length was available to construct at least five consecutive thirty-day averages, the Lilliefors Test, with the exception of one mill location, indicated that the thirty-day averages were normally distributed. This supported the use of the Central Limit Theorem. The 99th percentile level was then selected to estimate the maximum thirty day value at each mill using the following relationship:

Max. 30 Consec Day Value = $Mean_{30}$ + 2.33 S.D.₃₀

where, Mean₃₀ and S.D.₃₀ represent the mean and standard deviation of the thirty-day values.

The maximum thirty consecutive day variability factor was then established in the following manner:

Max. 30 Day Variability Factor = $\frac{\text{Mean}_{30} + 2.33 \text{ S.D.}_{30}}{\text{Long-Term Average}}$

B. NCASI Approach

The NCASI analysis incorporated a similar approach as presented in the Development Document to estimate the maximum day and maximum thirty consecutive day variability factors. NCASI used (a) a nonparametric statistical technique to develop the maximum daily value for BOD5 and TSS effluent quality and, (b) the Central Limit Theorem to estimate the maximum thirty consecutive day value. NCASI did expand on these two methods of estimating effluent variability as described in the following. (1) <u>Maximum Day Variability</u> - NCASI included in its assessment of treatment process daily discharges effluent variation at the 99.7 percentile level, as this represents an estimate of a one day occurrence in a 365 day event. EPA's use of the 99 percentile level essentially truncates the maximum daily values to approximately 3-4 days out of a year. Further, a lower tolerance level, 5%, (which represents a 95% confidence limit) was also added to the analysis recognizing that a higher degree of confidence (i.e., greater than 50%) should be associated with the maximum daily variability factor as the maximum daily discharge effluent limitations are a not-to-exceed upper bound on treatment system performance.

In addition, where data were available, greater percentile levels were used to estimate the one-in-a-three year occurrence, 99.9 percentile, and a one-in-a-five year occurrence, the 99.95 percentile. This recognizes that NPDES discharge permits which incorporate effluent variation are normally written for periods greater than one year and often for five years.

The daily data for BOD5 and TSS were tested for its adherence to a normal distribution using five goodness-of-fit tests rather than the one test used in the Development Document. Any decision to accept (or reject) the hypothesis that the daily data conformed to a normal, log normal, or shifted log normal distribution was based upon a majority agreement of the five tests at the five percent tolerance level. The goodness-of-fit tests used were the: (a) Anderson-Darling, (b) Watson, (c) Cramer von Mises, (d) Kolmogorov-Smirnov, and (e) Kuiper test procedures. <u>Reference 6</u> contains the background for the use of these test procedures.

When daily discharge data were found to adhere to one of the previously cited distributions, it was used to project the maximum daily discharge at the following estimated frequencies of occurrence:

| Probability of Occurrence | Percentile Level |
|---|---|
| 3-4 days per 365 days 1 day per 365 days 1 day per 3x365 days 1 day per 5x365 days | 99 (M+2.33 S.D.) 99.7 (M+2.75 S.D.) 99.9 (M+3.10 S.D.) 99.95 (M+3.27 S.D.) |
| M = Mean of Daily Data SD = Standard Deviation of Da | ta |

Figure 1 illustrates the use of nonparametric analysis for a daily BOD_5 discharge at the 99 and 99.7 percentile levels. It should be noted that the values selected for analysis were those at the 0.50 and 0.05 tolerance levels. In many cases, a sufficient number of data were not available to estimate the 99.7 percentile level at the 0.05 tolerance level. These are indicated in tables which follow as a "greater than (>) value."

NCASI BON-PABAMETRIC TOLERANCE AMALYSIS FOR MILL: 3032, Nov 1977-Nov 1978, 69 BOD (Klbs/day)

335

334

333

0.1129E+02

0.1123E+02

0.1118E+02

0.9424

0.9919

0.9772

NCASI NON-PARAMETRIC TOLERANCE ANALYSIS FOB HILL: 3032, Nov 1977-Nov 1978, 69 BOC (Klbs/day)

PART 1. ANALYSIS FOR 99TH PERCENTILE.

0.90

0.95

0.99

PART 2. ABALYSIS FOR 99.7TH PERCENTILE.

| R & NK { 1= LOW} | VALUE OP VARIABLE | PROBABILITY E | B OF VALUE KCEFDING PRECENTILE | | LUE CF NEIABLE | EXCEEDANCE FROBABILITY (WEIBULI) | PRCB OF VALUE FICEEDING 99.7 PERCENTILE |
|--------------------------|----------------------|---------------|--------------------------------------|-----------------|-------------------|--|---|
| 341 | 0. 1256E+02 | 0.003 | 0.0325 | 341 0.1 | 2562+02 | 0.003 | 0.3590 |
| 340 | 0.12528+02 | 0.006 | 0.1444 | | 252E+02 | 0.006 | 0.7273 |
| 339 | 0.1177E+02 | 0,009 | 0.3365 | | 177E+02 | 0.009 | 0.9157 |
| 338 | 0.11682+02 | 0.012 | 0.5557 | | 168E+02 | 0.012 | 0,9798 |
| 337 | 0.1156E+02 | 0.015 | 0.7429 | 337 0.1 | 156E+02 | 0.015 | 0.9960 |
| 336 | 0.1132E+02 | 0.018 | 0.8703 | | 132E+02 | 0.018 | 0.9994 |
| 335 | 0.11292+02 | 0.020 | 0,9424 | | | | |
| 334 | 0. 1123E+02 | 0.023 | 0.9772 | | , | | |
| 333 | 0.1118E+02 | 0.026 | 0.9919 | TOLEBANCE LEVEL | HIGHEST RA | NK VAIUE | CF ACTUAL |
| 332 | 0.1062E+02 | 0.029 | 0.9974 | FOR EXCEEDING | EXCEEDIN | G VABIAI | BLE TOLERANCE |
| 331 | 0.1056E+C2 | 0.032 | 0.9992 | 99.7 PERCENTILI | TOLEBANCE I | EVEL | IBVEL |
| TOLERANCE : FOR FICEE | DING EXCEEDIN | IG VABIABLE | ACTUAL Tolerance | 0.01 0.05 | GT 341 GT 341 | | |
| 99.0 PERCE | NTILE TOLÉBANCE I | EVEL | IEVEL | 0.10 | GT 341 | | |
| | | | | 0.30 | 341 | 0.12561 | |
| | | | | 0.50 | 340 | 0.12521 | |
| 0.01 | 341 | 0.1256E+02 | 0.0325 | 0.70 | 340 | 0.12521 | |
| 0.05 | 340 | 0.12528+02 | 0.1444 | 0.90 | 339 | 0.11771 | |
| 0.10 | 340 | 0.1252E+02 | 0.1444 | 0.95 | 3 38 | 0.11681 | |
| 0.30 | 339 | 0.1177E+02 | 0.3365 | 0.99 | 3 37 | 0.11561 | 8+02 0,9960 |
| 0.50 | 338 | 0.11682+02 | 0.5557 | | | | |
| 0.70 | 337 | 0.115EE+02 | 0.7429 | | | | |

ILLUSTRATION OF NON PARAMETRIC ANALYSIS FIGURE 1 AT THE 99 AND 99.7 PERCENTILE LEVELS

1 Ġ, 1

Figure 2 demonstrates the use of the goodness-of-fit tests as applied to a daily BOD5 discharge. A "yes" in the various goodness-of-fit test procedure columns rejects the hypothesis that the data comes from a normal distribution. A "no" does not reject the hypothesis that the data comes from a normal distribution. In this particular illustration, the daily BOD5 discharge data adhere to a log-normal distribution at the 0.05 significance level.

The selection process for classifying whether data conforms to a normal, log-normal or shifted log-normal distribution, is as follows. The order of selection used in this report is 1) normal, 2) log-normal and 3) shifted-log normal and is based on choosing the simplest distribution which shows no rejection.

Maximum Thirty Consecutive Day Analysis- NCASI adopted and (2) expanded upon the approach presented in the Development Document. In addition to using the "crunched data" form of the daily BOD5 and TSS data, the same data was left intact in its chronological order and a fixed, thirty-day window was used to scan the data for the thirty-day averages. This procedure is called the Fixed Start/ Fixed Window (FS/FW) technique. It generally resulted in at least one, to as many as seven additional, thirty-day observations over the crunched data method. In the FS/FW method, if there were less than twelve observations in the window, that estimate of thirty day performance was not included in the analysis. A feature of this method is it corresponds to the NPDES program, where the window may vary in size from 28 to 31 days. The fixed start (FS) aspect indicates that the analysis is initiated on the first day of the first month of the data record.

In addition to the use of the two procedures for estimating the maximum thirty consecutive day performance level, the BOD5 and TSS data were analyzed for the maximum average thirty consecutive day (MA30CD) value that exists in the data. This value is derived by a thirty-day window moving on the data as chronologically collected (i.e., data not crunched). This value was then compared with the statistical estimates made for the maximum thirty consecutive day average values.

The five goodness-of-fit tests cited previously were then used to determine if the 30 consecutive data (or day) averages conformed to a normal distribution as projected by the use of the Central Limit Theorem. Figure 3 illustrates the use of the five tests to analyze thirty-day BOD₅ averages for normality at the 0.05 significance level. In this particular example, the data appeared to fit a lognormal distribution rather than a normal distribution.

(3) Selection of Performance Data for Variability Analysis - The 96 mills representing both the combined EPA and NCASI data bases were reduced to 67 mills where variability analysis was conducted.

| NOLOT | | | | | |
|----------------|----------------|---------------------------------|----------------------------|---------------|--------|
| | | EILIY ANALYSIS 1978, 69 ECC | | | |
| PART 1. ORG | | (CRUNCHEE, ONI CCNESS CF FIT | | (VES) | |
| UNTRANS FOR ME | D DATA (NORMAI | DISTRIBUTION) | | | |
| NUM. OBS. | MEAN | STD DEV | SKEW (| OEF | |
| 341 | 0.5310E+01 | 0.2373E+0 | 0.797 | 2E+CD | |
| AN | D/DARLING | WATSON | CHAMER/VM | KCIMCGORCV | KUIPEE |
| VALUE | 5.759 | 0.735 | 0.924 | 1.735 | 2.962 |
| SIGNIF LEVEI | | | | | |
| 0.150 | YES | YES | YES | | YES |
| 0.100 | | YES | YES | YES | YES |
| | YES | YES | YES | YES | YES |
| 0.025 | | YES | YES | | YES |
| 0.010 | YES | YES | YES | YES | YES |
| LOG-10 TRANS | FORMED DATA (1 | LCG NOBMAL DIS | IFIEUTICN) | | |
| NOM. OBS. | MEA N | STE CEV | SKEW | COEF | |
| 341 | 0.6822E+00 | 0.1954E+0 | -0,894 | 1E-01 | |
| Al | ND/DAELING | WATSON | CEAMEF/VM | KOLMOGOROV | KUIPEE |
| VALUE | 0.700 | 0.105 | 0.106 | 0.745 | 1.452 |
| SIGNIF LEVEL | | | | | |
| | YES | YES | YES | NO | YES |
| | YES | YES | YES | NC | YES |
| 0.050 | - | NC | NC | NC | NO |
| 0.025 | NO | NC | NO | NO | NO |
| 0.010 | NO | NC | NO | NO | NO |
| SHIFTED LOG | -10 TRANSFORME | D DATA (SEIFTE | D ICG NCEMAL | DISTFIBUTION) | |
| SHIFT CON | STANT = -0 | .433 SMAILE | S" VALUE = | 1.269 | |
| NUM. OBS. | MEAN | STC CEV | SKEW | COEF | |
| 341 | 0.7230E+00 | 0.17ECE+C | c -0 . 1 92 | 0E-03 | |
| A | N D/DAELING | WATSON | CFAMER/VM | KCIMCGOPCV | KUIPER |
| VALUE | 0.805 | 0.124 | 0.124 | 0.856 | 1.561 |
| SIGNIF LEVEL | | | | | |
| 0,150 | YES | YES | YES | YES | YES |
| 0.100 | YES | YES | YES | YES | YES |
| 0.050 | YES | NC | YES | NO | YES |
| 0.025 | NC | NC | КC | NO | NC |
| 0.010 | NO | NC | NC | NO | NO |
| | FIGURE 2 | ILLUSTRATION TEST FOR | OF GOODNESS- DAILY DATA | -OF-FIT | |
| | | | | | |

| | - | | | | | | | | | | |
|------------|----------------------------------|-----------------------------------|-----------------|------------|------------|-----------------|----------------|-----------------------------------|-------------------|------------|-----------|
| | | | | | | | | | | | |
| | CASI EFFLUENT VARI | | t. . | | | #C1.87 | | | ~ | | |
| | 3005, Sep 1977-Sej | | |) | | POR HILL: 3005 | | FABILIY ANALYSI P 1978, 49 BOC | |) | |
| PART 2. | 30-VALUE AVEFAGI Summary CF (| S (CHUNCERT DA COCENESS OF FIG | | | | PART 3. 30- | | (FIXED START, Goodwess of Fit | | | |
| . UNTRANSE | PORMED DATA INCRM | L DISTRIBUTION |) | | | A. UNTRAUSFORE | ED DATA (NCENA | L DISTRIEUTION |) | | • |
| NUM. C | DBS. SEAN | STD DEV | SKEW | COEP | | NUM. OBS. | МЕАБ | STD LEV | SKBW | COPP | |
| 1 | 11 0.5106E+01 | 0.2977E+0 | 1 0.18 | 992+01 | | 12 | 0.5050E+01 | 0.26E1E+C | 1 0.143 | 332+01 | |
| | AND/DARLING | WATSON | CE ÀMFR/VM | KOLMOGOROV | KUIPEB | 1 | D/DARLING | WATSON | CBAHER/VM | KOIBOGOROV | KUIPER |
| VAL E | 1.003 | 0.132 | 0.145 | 0.780 | 1.521 | VALUE | 1,099 | 0. 148 | 0.161 | 0.797 | 1.518 |
| SIGNIF LE | VEL | | | | | SIGNIF LEVEL | | | | | |
| 0.150 | YES | Y ES | YES | YES | YES | 0.150 | YËS | YES | TES | YES | YES |
| 0.100 | TES | YES | YES | NO | TES | 0.100 | YES | YES | TES | NO | YES |
| 0.050 | TES TES | Y ES NC | TES TES | NO NO | TES No | 0.050 | YES Yes | TES TES | TES TES | BO No | YES No |
| 0.025 | TES NO | NC | NO | NO | NO | 0.010 | TES | | 165 | NO | 10 |
| | RANSFORMET DATA (| • • | | NO | NU | B. LOG-10 TRANS | | | | | |
| | | | | | | | | | | | |
| NUM. O | | STE LEV | SKEW | | | NUM. OBS. | BEAD | STC CEV | SKEW | | |
| 1 | 0.6562E+00 | 0.2106E+0 | 0 0.961 | 18E+00 | | 12 | D. 65682+00 | D. 2010E+00 | 0.831 | 32+00 | |
| | AN D/DABIJSG | WATSON | CFARER/VE | KOLHOGOBOV | KUIPEB | 83 | ND/DABI ING | WATSON | CBAHER/VN | KOLNOGOBOV | KUIPBB |
| VALUE | 0.413 | 0.049 | 0.053 | 0.509 | 0.994 | VALUE | 0,529 | 0.063 | 0.067 | 0.546 | 1.044 |
| SIGNIP LE | VEL | | | | | SIGNIF LEVEL | | | | | |
| 0.150 | NO | NC | BC . | NO | NO | 0.150 | NO | #C | NO | NO | EO. |
| 0.100 | NO | N O N | BC | BO | NO | 0.100 | NO | ₩C | BC . | NO | NO |
| 0.050 | NO | NC | NC . | NO | NO | 0.050 | NO | 90 90 | NO NO | NO | 80 |
| 0.025 | 80 80 | NC NG | NO NC | NO NO | 80 80 | 0.025 | FO FO | NC | 10 | NO NO | NO NC |
| 0.010 | | | | | 1 0 | | | | | • | |
| | LOG-10 TRANSPORME | • | | | | C. SHIFTED LOG- | | | | - | |
| SEIFT (| CONSTANT = 2 | . 372 SEALLE: | ST VALUE = | 2.646 | | SHIPT CONS | | | T VALUE = | 2.707 | |
| 905. O | DS. MEAN | STO CEV | SKEW | COEF | | NUM. OBS. | BEAD | STC CEV | SKEN | COEF | |
| 1 | 1 0.2102E+00 | 0.4835E+00 | 0,528 | 8E-03 | | 12 | 0.2035E+00 | 0.47252+00 | -0.775 | 22-04 | |
| | AND/DAPIING | WATSON | CF MER/VM | KOLMOGOBOV | KUIPEE | A X | D/DARLING | WATSON | C S & H B B / V H | KCLHOGOBOV | KOIPER |
| VALUE | 0.164 | 0.023 | 0.022 | 0.443 | 0.846 | VALUE | 0.212 | 0.026 | 0.025 | 0.450 | 0.859 |
| SIGNIF LE | | | | | | SIGNIF LEVEL | | | | | |
| 0.150 | NO | NC | NO | NO | NO | 0.150 | NO | BC . | 10 | NO | 80 |
| 0_100 | NC | NC | NO | NO | NO | 0.100 | 110 - | NC No | NO NC | NC NC | NO NO |
| 0.050 | NC | NC NC | KO NC | NO . NO | NO | 0.050 0.025 | NO - | NO | NC NO | NO | NO |
| 0.025 | NO NC | NC | NC NO | NO | NO | 0.025 | RC RC | NO | NO NO | #0 | NO |
| | p.c. | 1-0 | μÇ | F U | nU. | 3.010 | -~ | - | | | |
| 4 | | | | | | | | | | | |

FIGURE 3 ILLUSTRATION OF GOODNESS-OF-FIT TESTS FOR THIRTY DAY DATA -9-

Mills providing primary treatment, or insufficient frequency of data, were not included in this variability analysis; therefore, all variability cited in this review is associated with biological treatment processes. Mills not included in the variability analysis are identified in Table A3. Not all 67 mills' data were examined for both BOD5 and TSS effluent quality as some locations provided insufficient BOD5 and TSS data to warrant variability analysis.

One mill in the EPA data base was not used (ID No. 040011, Mill No. 49, Table A3) due to limited or zero BOD removal during several months of performance.

In addition, one mill (ID No. 030030, Mill No. 4, Table 3), which was included in the original EPA "verification mill" data provided by the E.C. Jordan Co., did not appear in the EPA Development Document variability analysis. A review of this mill's data indicated that it provided sufficient frequency for both BOD₅ and TSS effluent quality to warrant its use in the variability analysis.

Table A4 contains those mills finally selected for variability analysis along with their effluent quality. The mills marked with an asterisk are those that appear in the Development Document variability analysis with the exception of Mill No. 4. Those mill numbers which are underlined represent the data base used in this review of variability.

III RESULTS AND DISCUSSION

A. Daily Effluent Quality

Table A5 presents the results of the goodness-of-fit tests applied to the daily BOD5 and TSS discharges. Out of the 73 performance periods examined for BOD5 daily discharge, 3 indicated that the data were normally (N) distributed. Also, of 77 performance periods for TSS effluent quality, 2 demonstrated adherence to a normal distribution. The remaining performance periods for BOD5 and TSS indicated a similar distribution among the log normal (LN), shifted log normal (SLN) and nonidentified categories. These are summarized in Table 1.

| TABLE 1 | SUMMARY | OF STATISTIC | AL DISTRIBUTIONS |
|---------|---------|--------------|------------------|
| | OF | TREATED DAIL | Y DISCHARGES |

| No. of Performance Periods | Parameter | N | LN | SLN | Non- Identified |
|-------------------------------|------------------------|---|----|-----|--------------------|
| 73 | BOD5 | 3 | 19 | 20 | 31 |
| 77 | TSS | 2 | 21 | 24 | 30 |
| 12 | BOD ₅ & TSS | - | 6 | 7 | - |

It should be noted that the term "performance periods" is used in contrast to mill location as a number of mills provided more than one year's data. The performance period reflects approximately 12 months of data.

Six performance periods demonstrated adherence to a log-normal distribution for both BOD₅ and TSS while seven periods indicate that a shifted log normal distribution fit both BOD₅ and TSS discharges. This was expected because NCASI believes the source of variability is different for each of these parameters.

As the daily data did not demonstrate a predominant adherence to any of the three distributions, the use of a nonparametric statistical analysis for the daily data is a reasonable alternate for estimating a maximum daily value. However, almost two-thirds of the performance periods fit at least one of the three distributions and this observation is used in subsequent analyses to compare with the nonparametric method.

Tables A6 and A7 summarize the analyses provided to estimate the maximum daily variability factors for both BOD5 and TSS. The factors were derived from three analytical techniques: (a) the use of nonparametric analyses at the 50% and 5% tolerance limits at percentiles of 99, 99.7, 99.9 and 99.95, (b) the use of the distribution functions (i.e., N, LN, or SLN where applicable) to estimate the daily effluent quality at the same percentile levels, and (c) the use of the actual observed maximum daily values from the individual performance period data.

The variability factors were calculated by dividing the various maximum daily discharge values by the long-term means. Some observations made from these analyses are as follows:

(1) The use of a nonparametric analysis at the 99 percentile level with a 50% tolerance level (or 50% confidence limit) should be modified. By its very nature, the 99 percentile level provides a probability of occurrence that 3 to 4 days of a year will exceed this level. The shortcoming in this approach is evident when one compares this estimate with the observed maximum daily values. In addition, the use of a 50% tolerance limit indicates that a variability factor based upon a specific percentile has a probability of being less than (low) 50 percent of the time. NCASI evaluated an appropriate alternate to the EPA technique by using the 99.7 percentile level, at the 5% tolerance level (or 95% confidence limit). The 99.7 represents a once-in-a-year occurrence while the 5% tolerance level suggests that the variability factor has a 95 percent probability of being correct.

(2) Maximum daily discharges for BOD₅ and/or TSS which adhered to one of the statistical distributions, insofar as they were tested, were projected for their occurrence at frequencies of once in a year (99.7), once in three years B99.9) and once in five years B99.95). NCASI determined that the maximum day variability factors calculated for these return periods were greater than the factors calculated using the EPA nonparametric method. This suggests that a data base for effluent quality of at least three to five years should be examined for variability especially since permitted effluent quality and its variation are typically specified for these periods in the NPDES program.

B. Thirty Consecutive Day Variability

The daily data for BOD5 and TSS in thousands of pounds per day (klbs/day) were assembled in consecutive thirty day periods by two methods. One method, referred to as the "Crunched Data" (CD) technique, squeezed the data together when there were any voids or missing data in order to provide a continuous record. This is the procedure used by EPA in the Development Document. The consecutive thirty values were then averaged for each mill and examined by the five goodness-of-fit tests (previously cited) to see if the averaged thirty day values were normally distributed. As noted earlier, the Development Document analysis used one goodness-of-fit test, referred to as the Lilliefors Test, to assess the averaged thirty day values for normal distribution.

The second approach used by NCASI is referred to as the "Fixed Start/Fixed Window" (FS/FW) method for developing the consecutive thirty day averages. This method fixed the start of consecutive thirty day windows at the first day of the first month of the data record. The data that appeared in each window were then averaged to construct the 30 day estimates of effluent quality. These averages were then analyzed for normal distribution using the five goodnessof-fit tests. The reasons for considering the FS/FW approach were mentioned earlier in this report.

In addition, the data record for BOD_5 and TSS at each mill location was then analyzed for the actual maximum average thirty consecutive day (MA30CD) value. Due to the procedure used in both the "crunched data" and "fixed start/ fixed window" methods, a possibility exists that the actual MA30CD value is split between consecutive windows in the averaging process. Basically, the actual MA30CD value is a logical test value for the adequacy of using the 99th percentile value for estimating the maximum thirty consecutive day value. Use of the 99th percentile is based upon a concern for committing, in statistical terms, a Type I error, which results from the rejection of a hypothesis, when indeed, the hypothesis is true. In this particular application, there was a concern for rejecting the hypothesis that the 30 day means were normally distributed, when indeed, it should be accepted (2). The Central Limit Theorem provides the basis that such means are normally distributed and for that reason, a high degree of confidence, 99th percentile, was used.

As noted earlier in this report, the goodness-of-fit tests were used to determine if the thirty day averaged value conformed to a normal distribution as proposed by the use of the Central Limit Theorem. <u>Table A8</u> presents the results of the goodness-of-fit test procedures for the thirty consecutive day BOD5 and TSS effluent quality. As can be seen, a substantial number of the thirty consecutive day performance periods adhere to a normal distribution. Essentially, all the remaining periods conformed to a normal distribution when the logarithm (with or without a shift constant) of the thirty day averages was examined. The following <u>Table 2</u> is a summary of the individual distribution analysis appearing in Table A8.

| Performance | | CI | METH | HOD | F | S/FW | MET | HOD | |
|-------------|-------------|----------|---------|--------|--------|----------|----------|--------|--------|
| Periods | Parameter | N | LN | SLN | NO FIT | N | LN | SLN | No FIT |
| 72 77 | BOD5 TSS | 58 68 | 10 5 | 4 3 | - 1 | 57 62 | 12 12 | 3 1 | - 1 |

| TABLE | 2 | SUN | IMARY | \mathbf{OF} | THIRTY | DAY | PEF | FORMANCE |
|-------|---|-----|-------|---------------|--------|-------|-----|-----------|
| | | FOR | SELEC | TEL | DISTR | IBUTI | LON | FUNCTIONS |

As can be seen, agreement exists in most cases between the crunched data (CD) and fixed start/fixed window (FS/FW) methods of analysis. A greater number of the TSS 30 consecutive day averages conformed to a normal distribution than did the BOD data. NCASI's analysis did not produce the same degree of conformity to the normal distribution as the EPA analysis. In EPA's analysis one mill's data out of approximately thirty did not indicate a fit to a normal distribution. Therefore, analyses by both groups shows the Central Limit Theorem describes a majority of the cases. Tables A9 and A10 contain the results of the statistical estimates for the thirty consecutive day effluent quality for BOD5 and TSS, respectively. As noted previously, the estimate for the maximum thirty consecutive day value is calculated by adding the long-term average to the (2.33 x Standard Deviation) value. The variability factor is then calculated by dividing this value by the long-term average. In addition, the actual MA30CD values for the BOD5 and TSS data were also included for comparison with the estimated values for maximum thirty consecutive days. Both the crunched data and fixed start/fired window methods are used. Three estimates for the thirty-day variability factors are presented for the combined EPA and NCASI data base.

As can be seen from <u>Tables A9</u> and <u>A10</u>, an array of variability factors are developed from the three methods. Initially, the data appearing in these tables were reviewed for differences in the variability factors calculated using the crunched data (EPA) method and the fixed start/fixed window (NCASI) alternate method. This comparison is summarized in Table 3.

| TAI | | I THIRTY-DAY VA ON OF FS/FW ME | | |
|------------------------|-------------------------|-----------------------------------|----------|----------------------|
| Performance Periods | Parameter | FS/FW > CD | FS/FW=CD | <u>FS/FW < CD</u> |
| 70 73 | BOD ₅ TSS | 33 40 | 7 9 | 30 24 |

The performance periods represent the approximate twelve month data time frames in <u>Tables A9</u> and <u>A10</u> and do not include the multiyear data records. The NCASI FS/FW method produced greater maximum 30 consecutive day variability factors than the EPA CD method in 33 out of 70 performance periods for BOD₅ effluent quality and 40 out of 73 performance periods for TSS effluent quality.

The MA30CD values for BOD5 and TSS data were used to test the adequacy of both CD and FS/FW methods to project (estimate at the 99th percentile) their respective estimates for maximum thirty consecutive day performance. Once again, the MA30CD value represents the actual value as contrasted to the statistical projections using the CD and FS/FW methods. Again Tables A9 and A10 were reviewed to determine the degree to which the variability factors estimated from the FS/FW and CD methods compared with actual performance. This is summarized in Table 4.

| TABLE 4 | COMPARISON OF | VARIABILITY | FACTORS | ESTIMATED BY |
|---------|---------------|-------------|-----------|--------------|
| | FS/FW AND CD | METHODS WIT | TH THE MA | A30CD VALUE |

| Periods | Parameter | | CD Metho (<u>=MA30CD</u>) | d (<u><ma30cd< u="">)</ma30cd<></u> | FS/F (<u>>MA30CD</u>) (| W Metho | |
|---------|-----------|----|--------------------------------|---|---------------------------------|---------|----|
| 70 | BOD5 | 30 | 3 | 37 | 39 | 2 | 29 |
| 73 | TSS | 43 | 1 | 29 | 44 | 4 | 25 |

The FS/FW method, as indicated in <u>Table 4</u> produced variability factors for BOD₅ which were greater than the MA30CD variability factors in 39 of the 70 performance periods as compared to 30 out of 70 for the CD method. The FS/FW technique calculated variability factors which were greater than the MA30CD values in 44 out of the 73 performance periods for TSS as compared to 43 out of 73 for the CD method.

The selection of the averaging method, CD vs FS/FW, appears to be an important element in estimating monthly variability for the data base used in this analysis. The fixed start/fixed window method (FS/FW) is certainly a viable alternate to the crunched data (CD) method used in the EPA analysis presented in the Development Document. The FS/FW method does not differ from the statistical treatment of the data in that its approach is based upon the Central Limit Theorem. Most importantly, the FS/FW method is similar to the NPDES reporting period where the actual "window" (i.e., monthly performance periods) varies from 28 to 31 days.

C. Development of EPA Proposed Variability Factors

EPA reviewed the data of the verification mills (30 and 31 mills for maximum thirty consecutive day variability for BOD5 and TSS, respectively; and 35 mills for maximum day variability for both BOD5 and TSS) and computed their performance on an annual average basis for BOD5 and TSS. These annual averages were used to determine if the individual mill treatment systems met a specified level of performance such as BPT or the proposed BCT effluent limitations. The maximum day and maximum thirty consecutive day variability factors were then assembled for four levels of treated effluent quality, (a) mills with biotreatment, (b) mills with effluent quality better than BPT limitations, (c) mills with biotreatment discharging effluent quality better than BPT, and (d) mills with biotreatment exceeding BCT (proposed) limitations. The variability factors were then averaged within these four levels. The variability of mills falling into the preceding 2,3, and 4 categories was then reviewed and resulted in the following variability factors being proposed by EPA for BCT technology.

TABLE 5VARIABILITY FACTORSBCT TECHNOLOGY(Options 1 & 4)

| Production Subcategory | Maximum 30 Consecut | ive Day Maximum Day |
|---|-----------------------------|-----------------------------|
| | BOD ₅ <u>TSS</u> | BOD ₅ <u>TSS</u> |
| All Industry Subcategories with the exception of the following: | s 1.78 1.82 | 3.00 3.00 |
| NonInt-Tiss. - Ligtwt. - Filt/NW - Papbd. | 1.82 1.76 | 3.25 3.60 |

EPA concluded that the maximum thirty consecutive day values were similar to those developed for the previous Phase II BPT effluent limitation and therefore proposed that they be used for BCT technology. However, the maximum daily factors, developed from the variability analysis in the Phase III Development Document, were less than the existing BPT Phase II factors. EPA proposed the lower value of 3 (ratio of maximum day to annual average) for the maximum day variability factor. Exception to this approach were four subcategories in the nonintegrated subcategories shown in Table 5. The factors proposed for these mills are the same as BPT variability.

D. Summary of NCASI Analysis

The variability factors for the 70 plus performance periods presented in Tables A9 and Al0 were averaged and summarized in Table All. Several differences between the NCASI and EPA average factors are evident. First, the average maximum day variability factors produced by two of the analytical methods are greater than the proposed BCT factor of 3.00 for both BOD5 and TSS discharges. The variability factors developed using the nonparametric analysis at the 50 percent tolerance level (NPA, 99%, 50% TL) are below EPA's proposed factors. However, EPA's method truncates the daily variability by its very nature in representing a probability of occurrence that is expected to be exceeded 3 to 4 days in a year at a 50% level of confidence. This becomes evident when EPA's value is compared with observed data derived from actual maximum daily values as shown in Table All. Although the use of the nonparametric analysis at the 99.7 percentile at the 50% tolerance level produces a closer agreement with observed daily variability factors, it still results in variation less than observed in actual treatment system performance. Because maximum daily limitations are specified as a not-to-exceed upper bound in system performance, the use of the 99.7 percentile level at the 5% tolerance level (i.e., 95% confidence

limit) should be seriously considered. This would allow the development of a maximum daily variability factor representative of a once-in-a-year occurrence in which there is 95% confidence that the variation is less than projected. This analysis was attempted in this review; however, a year's data (365 observations) were generally insufficient to estimate the 5% tolerance level. (See <u>Tables A6</u> and A7.)

The averaged maximum thirty consecutive day variability factors (see <u>Table All</u>) resulting from NCASI analysis are greater than those proposed for BCT technology. Both crunched data (CD) and fixed start/fixed window (FS/FW) methods projected variability factors greater than that observed in actual treatment process performance. The FS/FW method produced a variability factor which was equal to or slightly greater than the CD (or EPA) method.

Since beginning this analysis, NCASI has received supplementary data from EPA's contractor. These data arrived too late in May to adequately test a number of longer term records for projection of 99.7% probability at the 5% tolerance level. However, these analyses will be performed following June 9, 1981 and will be submitted with comments on BCT methodology. In the meantime, NCASI has reviewed the variation in effluent quality for two mills meeting BPT which have long data records. Further, NCASI has examined the variation in effluent quality using the extreme values from the data base examined in this report. In other words, NCASI has examined the variation in the variability of biological treatment systems. Both of these analyses are presented in the following section.

IV DEMONSTRATED VARIATION IN EFFLUENT QUALITY VARIABILITY

A limited number of mills in the NCASI data base used in this review provided several years of process performance data. Mill No. 2, a bleached kraft dissolving pulp mill, provided five years of data while Mill No. 39, a semichemical mill contributed three years of data. Effluent quality from the treatment processes located at these two mills has been compared to BPT effluent limitations for the three specified time frames for system performance; annual average, maximum thirty day, and maximum day. This comparison is presented in <u>Table Al2</u>, along with other mills used in this review. As indicated, Mill No. 2 met BPT effluent quality for both BOD₅ and TSS for all time frames during the five year period. Mill No. 39 met BPT requirements for the last two years of the data record. The first year complied with BPT limitation for BOD5 and missed compliance with TSS limitations by only 0.7 lb/ton in its MA30CD value; however, the maximum daily TSS limitations were attained during this period.

Table A13 presents a summary of the multiyear performance at Mills 2 and 39 along with the variation in effluent quality variability projected by the statistical procedures used in this review and the variability demonstrated in the actual BOD5 and TSS effluent quality. Examination of the variability factors presented in the "Observed" columns indicates a range in variability factors experienced at these mill locations for both BOD5 and TSS effluent quality.

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Of particular interest at Mill No. 2 is that the performance period (2-2) producing the best effluent quality (annual average basis) had the highest variability factors for both BOD₅ and TSS discharge, exceeding those recommended in the EPA Development Document.

Mill No. 39 presents an interesting contrast in variability. Two separate years (39-2, 39-3) of almost identical annual average performance produced variability factors which were less than the proposed BCT factors in one and greater than the proposed factors in the other year.

The data appearing in <u>Table A13</u> readily supports the need to examine multiyears of treatment system process performance data in order to adequately address the range in effluent quality experienced in treatment systems operating in the pulp and paper industry.

A preliminary analysis of the range in variability factors was conducted on the factors developed in this review. The data appearing in Tables A6, A7, A9, and A10 were analyzed to determine if the variability factors conformed to a statistical distribution which could be used to project to a given probability of occurrence, say the 95% level. The same goodness-of-fit test procedures as described earlier were used to test the variability data for adherence to a normal distribution. It is emphasized that this procedure was used as a projective technique to provide a degree of confidence in assigning a variability factor to process performance rather than simply averaging the variability factors as was done in the EPA analysis. The basis for this approach is the preceding discussion. The results of this analysis are summarized in Table 6.

| TABLE 6 | ESTIMATE | OF | 95% | PROBABILI | ITY OF |
|---------|------------|------|-----|-----------|---------|
| | OCCURRENCE | E OF | VAI | RIABILITY | FACTORS |

| Analysis _Method | Ratio of Max. Day to Long-Term Average | | | | | | | | |
|---------------------|---|------|------|------|----------------------|----------|---------|--|--|
| | (AA) | | (| 95%) | (Distribution Basis) | | | | |
| | BOD | TSS | BOD | TSS | | | | | |
| NPA (99%) | 2.85 | 2.91 | 4.13 | 4.61 | N/BOD, | LN/TSS, | 1% S.L. | | |
| NPA (99.7%) | 3.35 | 3.42 | 5.45 | 4.92 | LN/BOD, | SLN/TSS, | 1% S.L. | | |
| Observed Data | 3.61 | 3.83 | 6.02 | 6.25 | LN/BOD, | SLN/TSS, | 1% S.L. | | |

| | | | | | , 30 Day Average | | |
|------------------------------------|----------------------|----------------------|----------------------|----------------------|---|-----------|--|
| | (A | A) | (95%) | | (Distribution Basis) | | |
| | BOD | TSS | BOD | TSS | | | |
| Crunched Data FS/FW Observed | 1.98 1.99 1.91 | 1.91 1.98 1.82 | 2.33 2.24 2.78 | 2.05 2.13 2.65 | SLN/BOD, LN/TSS, SLN/BOD, SLN/TSS LN/BOD, SLN/TSS | , 1% S.L. | |

S.L. = Significance Level

AA = Arithmetric Average

95% = 95% Probability of Occurrence of Var. Factor Projected from Distribution Fit. Equals Mean + 1.65 (Standard Deviation)

The range in variability factors from greater than seventy performance periods fit at least one of the normal distributions used in the review, normal (N), log normal (LN), or shifted log normal (SLN). The fit of the data to the specific distribution was used to project the 95% probability of occurrence of the variability factors. The analysis of the maximum day variability factors indicates that a factor equal to or greater than four is to be expected with a 95% degree of confidence. Although this is higher than the maximum day variability factor (VF) of 3 proposed by EPA for BCT technology, a VF of four would still not represent all the observed variation of the mills providing multiyear data shown in Table Al3.

The 95% probability of occurrence of the maximum thirty consecutive day variability factors was estimated to be at least 2.1 as shown in the table above. This degree of effluent variation was greater than the EPA proposed values of 1.78 for BOD₅ and 1.82 for TSS but, once again, does not reflect all the variability of the multiyear data presented in Table A13.

The preceding analysis indicates that the variability factors conform to a distribution which can be used to provide a greater degree of confidence than the average value approach used by EPA in proposing variation for BCT technology. Estimating the probability of occurrence of variability factors should be expanded by EPA to the possible use of "extreme value" distribution functions such as the Gumble or log Pearson Type III.

V CONCLUSIONS

A review of more than 70 performance periods (each with approximately 12 months of data) for biological treatment processes operating in the pulp and paper industry suggests modifications to the EPA methodology used in developing maximum day and maximum thirty consecutive day variability factors for BOD₅ and TSS discharges as follows:

(1) The use of non-parametric statistical analysis (NPA) for maximum daily variation should at least incorporate the 99.7 percentile. This percentile level represents the approximate occurrence of one day in a year. The current use of the 99 percentile level by EPA provides a probability that a maximum daily value could be expected to be exceeded 3-4 days in a year.

(2) The use of a 5% tolerance level (or a 95% confidence limit) should be used in the nonparametric approach to daily variation. This would provide a 95% degree of confidence in the estimate of the variability factor rather than a 50% degree of confidence as presently proposed.

(3) The use of goodness-of-fit test procedures should be expanded to include additional test procedures. The use of one test procedure to determine if a series of events is normally distributed may be incomplete.

(4) Statistical distributions characterizing daily discharge quality should be used to project variability to time frames of greater than one year because NPDES permitted daily discharges are not-to-exceed values generally in effect for up to five years.

(5) The actual (observed) effluent quality (maximum day and maximum thirty day) should be compared to the values projected by statistical techniques and greater effort should be placed on rectifying predicted values which are lower than observed values.

(6) The Central Limit Theorem used by EPA appears to be an adequate approach to estimate maximum thirty day effluent quality variability. The "crunching of data" to provide thirty consecutive values should be replaced by a "fixed start/fixed window" alternate. Longer data sets should be examined for mills which require additional data to more fully describe monthly averages. (7) Biological treatment processes exhibit a range of variability in effluent quality from year to year and from system to system. Averaging variability factors does not adequately account for the system to system and year to year situation.

(8) Variability factors should be developed to reflect a specific probability of occurrence, e.g. 95% confidence limit, to account for observed variability that can be expected to occur in a five year time period. Initial analysis of the range in variability factors indicates an adherence to statistical distributions, predominantly log-normal or shifted log-normal. Use of this observation suggests that a maximum daily variability factor equal to or greater than 4 and a maximum thirty consecutive day variability factor equal to or greater than 2.1, could be used to predict effluent variation at a 95% degree of confidence.

(9) Analysis of multiyear data provided by two mills, achieving BPT and approaching or exceeding proposed BCT limitations, shows that a range in variability factors exists from year to year. In these specific cases, variability factors exceeded the factors proposed for BCT technology.

VI LITERATURE REFERENCES

- (1) "Development Document (Proposed) for Effluent Limitations Guidelines and Standards for the Pulp, Paper and Paperboard and the Builders' Paper and Board Mills - Point Source Categories," U.S. E.P.A., E.P.A. 440/1-80/025b, November-December 1980.
- (2) "Technical Data Generation, Volume 117, Item 9-6, Statistical Analysis," Document obtained from EPA public record for proposed Effluent Guidelines for the Pulp and Paper industry.
- (3) Ang, A.H.-S. and Tang, W.H., "Probability Concepts in Engineering Planning and Design, Volume I Basic Principles," John Wiley and Sons, 1975.
- (4) Bradley, J.V., "Distribution-Free Statistical Tests," Prentice-Hall, 1968.
- (5) Gibbons, J.D. "Nonparametric Statistical Inference," McGraw-Hill, 1971.
- (6) Stephens, M.A., "EDF Statistics for Goodnes of Fit and Some Comparisons," Journal-American Statisticsl Association, Vol. 69, No. 3, September, 1974.

APPENDIX A

TABLES A1 THROUGH A13

| TABLE Al | VARIABILITY EXPRES | SSED IN | PULP | AND | PAPER |
|----------|--------------------|---------|------|-----|-------|
| | INDUSTRY EFFI | | | | |

| | | RATIO ⁵ | | | TSS | | | |
|--|----------------------------|--------------------|------------------|------------------|------------------|------------------|--|--|
| CATEGORY | MD/AA MA30 | | OF: MD/MA30CD | MD/AA MA | RATIO 30CD/AA | OF: MD/MA30CD | | |
| (PHASE-I) | BEST PRACTICABLE TREATMENT | | | | | | | |
| UBK | - | - | 2.0 | - | - | 2.0 | | |
| NSSC(Na) NSSC(NH ₂) | · • | - | 2.0 | - | - | 2.0 2.0 | | |
| UBK-NSSC | - | _ | 2.0 | - | - | 2.0 | | |
| PAP. BD | - | - | 2.0 | - | - | 2.0 | | |
| (PHASE-II) | | | | | | | | |
| DISS KRAFT | 3.44 | 1.78 | 1.93 | 3.38 | 1.81 | 1.86 | | |
| BL.KR-MKT | 3.43 | 1.79 | 1.92 | 3.38 | 1.82 | 1.85 | | |
| BL.KR -BCT | 3.41 | 1.78 | 1.92 | 3.38 | 1.82 | 1.86 | | |
| BL.KR-FINE | 3.48 | 1.80 | 1.93 | 3.36 | 1.80 | 1.86 | | |
| SULFPAPER (BLOW PIT) | 3.42 | 1.78 | 1.92 | 3.38 | 1.82 | 1.86 | | |
| SULFDISS. | 3.42 | 1.78 | 1.92 | 3.38 | 1.82 | 1.86 | | |
| GROUND WOOD-CHEM/MECH. | 3.42 | 1.78 | 1.91 | 3.38 | 1.82 | 1.85 | | |
| GROUND WOOD-TMP GROUND WOOD-CMN | 3.42 | 1.79 | 1.91 | 3.38 | 1.82 | 1.86 | | |
| GROUND WOOD-CMN GROUND WOOD-FINE | 3.39 3.43 | 1.77 1.80 | 1.91 1.90 | 3.40 3.41 | 1.83 1.83 | 1.83 1.83 | | |
| GROUND WOOD-FINE | J. 4 J | 1.00 | 1.90 | · 3 • 4 T | 1.02 | 1.03 | | |
| SODA | 3.43 | 1.78 | 1.93 | 3.38 | 1.82 | 1.86 | | |
| DEINK | 3.42 | 1.77 | 1.93 | 3.38 | 1.82 | 1.86 | | |
| NONINT-FINE | 3.42 | 1.77 | 1.93 | 3.38 | 1.82 | 1.86 | | |
| TISS | 3.26 | 1.79 | 1.82 | 3.60 | 1.75 | 2.05 | | |
| TISS (WST.PAP.) | 3.43 | 1.78 | 1.93 | 3.38 | 1.82 | 1.85 | | |
| SULF-PAPER(DRUM WASH) | 3.42 | 1.78 | 1.92 | 3.38 | 1.82 | 1.86 | | |
| SULF-MKT PULP | - | - | 1.92 | - | - | 1.86 | | |
| AVG-PHASE II | 3.42 | 1.78 | 1.92 | 3.38 | 1.82 | 1.86 | | |
| | PROPOSED | BEST | CONVENTIONAL | TREATMENT | (OPTIONS | 51&4) | | |
| Above Categories With the Exception of the Following | 3.00 | 1.78 | 1.68 | 3.00 | 1.82 | 1.65 | | |
| NONINT-TISS | 3.25 | 1.79 | 1.82 | 3.60 | 1.76 | 2.05 | | |
| | 11 14 | 91 91 | 11 | H | n | •• | | |
| " -FILT/NW " -PAPBD | " | м | | | 1 | | | |
| 1 11 00 | | | | | | | | |

AA = ANNUAL AVERAGE, MD = MAXIMUM DAY, MA30CD = MAXIMUM THIRTY CONSECUTIVE DAY AVERAGE

TABLE A2BPT AND BCT (PROPOSED) EFFLUENT LIMITATIONSFOR THE PULP AND PAPER INDUSTRY

(LBS/TON)

| Prod. Category | (BPT) | ID (BCT) | BOI MA3((BPT) | <u>o</u> Śp | <u>AA</u> (BPT) (| | (BPT) | D (BCT) | TSS MA30CI (BPT) | D BCT) | AA (BPT) | |
|--------------------------|---------------|-------------|----------------------|-------------|----------------------|------|-------|------------|------------------------|-----------|-------------|------|
| BK-DISS | 47.2 | 24.4 | 24.5 | 14.4 | 13.8 | 8.2 | 74.6 | 37.2 | 40.1 | 22.6 | 22.1 | 12.4 |
| " - MKT | 30.9 | 21.0 | 16.1 | 12.4 | 9.0 | 7.0 | 60.8 | 26.4 | 32.8 | 16.0 | 18.0 | 8.8 |
| " - BCT | 27.3 | 15.0 | 14.2 | 9.0 | 8.0 | 5.0 | 48.0 | 21.6 | 25.8 | 13.2 | 14.2 | 7.2 |
| " - FINE | 21.2 | 11.8 | 11.0 | 7.0 | 6.1 | 4.0 | 44.3 | 18.4 | 23.8 | 11.2 | 13.2 | 6.2 |
| " - SODA | 27.4 | 11.8 | 14.2 | 7.0 | 8.0 | 4.0 | 49.0 | 18.4 | 26.4 | 11.2 | 14.5 | 6.2 |
| UBK-LNBD | 11.2 | 7.0 | 5.6 | 4.0 | - | 2.4 | 24.0 | 13.4 | 12.0 | 7.4 | - | 4.1 |
| " -CP | 11.2 | 9.0 | 5.6 | 5.4 | - | 3.0 | 24.0 | 15.4 | 12.0 | 8.8 | - | 4.8 |
| SEMI-Na. | 17.4 | 10.6 | 8.7 | 6.2 | - | 3.6 | 22.0 | 14.4 | 11.0 | 8.8 | - | 4.8 |
| CHEM NH3 | 16.0 | 10.6 | 8.0 | 6.2 | - | 3.6 | 20.0 | 14.4 | 10.0 | 8.8 | - | 4.8 |
| UBK/SEMI Chem | 16.0 | 10.6 | 8.0 | 6.2 | - | 3.6 | 25.0 | 17.4 | 12.5 | 10.6 | - | 5.8 |
| SULF. DISS NIT | 82.8 | 82.8 | 43.1 | 43.0 | 24.2 | 24.2 | 141.3 | 141.2 | 76.1 | 76.0 | 41.8 | 41.8 |
| SULF. DISS VIS | | 88.6 | - | 46.2 | • | 26.0 | - | | - | - | Π. | • |
| SULF. DISS CELL | n | 96.2 | * | 50.0 | n | 28.2 | • | | - | n | * | Ħ |
| SULF. DISS ACE | 91 | 104.0 | M | 54.2 | 77 | 30.4 | • | | - | | • | |
| SULF-PAP (100%) | - | 53.0 | - | 32.4 | - | 18.2 | - | 88.6 | - | 53.0 | - | 29.1 |
| SULF-PAP BLOW PIT | 63.6 | - | 33.1 | - | 18.6 | - | 87.9 | - | 47.3 | - | 26.0 | - |
| SULF-PAP DRUM WASH | 53.4 | - | 27.8 | - | 15.6 | - | 87.9 | - | 47.3 | - | 26.0 | - |
| SULF-PAP MKT | 80.0 | - | 41.7 | - | - | - | 99.0 | - | 53.3 | - | - | - |
| GNDWD-TMP | 21.2 | 7.8 | 11.1 | 4.6 | 6.2 | 2.6 | 31.1 | 12.4 | 16.7 | 7.4 | 9.2 | 4.2 |
| " CMN | 14.9 | 9.0 | 7.8 | 5.4 | 4.4 | 3.0 | 25.5 | 12.6 | 13.7 | 9.0 | 7.5 | 4.2 |
| " FINE | 13.7 | 8.2 | 7.2 | 4.8 | 4.0 | 2.8 | 23.5 | 11.8 | 12.6 | 7.0 | 6.9 | 4.0 |
| CHEM-MEC | H 27.0 | - | 14.1 | - | 7.9 | - | 39.5 | - | 21.3 | - | 11.7 | - |
| DEINK-FINE | 36.2 | 17.8 | 18.8 | 10.6 | 10.6 | 6.0 | 48.1 | 25.0 | 25.9 | 15.2 | 14.2 | 8.4 |
| " -TISS | n - | 19.6 | M | 11.6 | - | 6.6 | | 30.0 | | 18.2 | | 10.0 |
| WSTPAP-TISS | 27.4 | 13.2 | 14.2 | 7.8 | 8.0 | 4.4 | 34.1 | 15.6 | 18.4 | 9.4 | 10.1 | 5.2 |
| " -BD | 6.0 | 2.4 | 3.0 | 1.48 | - | 0.84 | 10.0 | 3.0 | 5.0 | 1.78 | - | 0.98 |
| " -MP | 8.0 | 3.6 | 4.6 | 2.2 | 2.6 | 1.2 | 21.6 | 7.0 | 11.6 | 4.1 | 6.4 | 2.4 |
| BLDG. PAP & ROOF.FLT, | | 10.00 | - | 6.0 | - | 3.2 | - | 10.0 | - | 6.0 | - | 3.2 |

BPT AND BCT (PROPOSED) EFFLUENT LIMITATIONS TABLE A2 FOR THE PULP AND PAPER INDUSTRY

(LBS/TON) (Cont'd)

| | rod. | | | | <u>0</u> 20 | | | (BPT) | | TSS MA30C | - | (BPT) | |
|------|---------|-------|-------|-------|-------------|-------|-------|-------|-------|--------------|------|-------|------|
| Lat | egory | (BPT) | (BCT) | (BPT) | (BCT) | (BPT) | (BCI) | (BPT) | (BCT) | (BPT) | BCT) | (BP1) | BCIJ |
| NONI | NT-FINE | 16.4 | 7.8 | 8,5 | 4.6 | 4.8 | 2.6 | 22.0 | 8.2 | 11.8 | 5.0 | 6.5 | 2.8 |
| ** | -TISS | 22.8 | 18.8 | 12.5 | 10.4 | 7.0 | 5.8 | 20.5 | 17.0 | 10.0 | 8.2 | 5.7 | 4.8 |
| " | -LGHT | 47.8 | 37.8 | 26.2 | 20.8 | 14.8 | 11.9 | 43.2 | 33.8 | 21.2 | 16.6 | 12.0 | 9.4 |
| n | -ELEC | 75.8 | 65.5 | 41.6 | 36.2 | 23.2 | 20.2 | 68.0 | 59.0 | 33.4 | 28.8 | 19.0 | 16.4 |
| * | -FILT | 58.8 | 46.8 | 32.4 | 25.8 | 18.2 | 14.4 | 53.2 | 42.0 | 26.0 | 20.6 | 15.8 | 11.8 |
| | -BD | 12.6 | 12.6 | 7.0 | 7.0 | 4.0 | 4.0 | 11.6 | 11.6 | 5.6 | 5.6 | 3.2 | 3.2 |

MD = Maximum Daily MA30CD = Maximum Average for Thirty Consecutive Days AA = Annual Average * = Annual Average Values Apply to Non-Continuous Dischargers

| TABLE A3 | MILL LOCATIONS PROVIDING DATA |
|----------|-----------------------------------|
| | REVIEWED FOR VARIABILITY ANALYSIS |

| Mill No. | ID No. ³ | Produc Catego | | Treatment Process | Data Time Frame | Comment |
|-----------------|---------------------|------------------|--------|----------------------|--------------------|---------------|
| 1 ^{*2} | 032001 | BL.KR. | -DISS. | AST | 7/78-7/79 | |
| 2 | 08501 | n | н | ASB/PS (ST) | 1/76-12/80 | |
| 3 | 34403 | N | H | AST | 9/77-7/79 | |
| 4 * | 030030 | BL.KR. | -МКТ. | ASB/PS | 8/77-8/78 | |
| 5 | 030005 | 11 | 11 | ASB/PS | 9/77-9/78 | |
| 6 | 08301 | 11 | 11 | ASP/PS(ST) | (1-12)/79 | |
| 7 | 19305 | 11 | 10 | AST (HYBRID) | (1-12)/79 | |
| 8 | 31107 | " | 11 | ASB/PS | 4/76-2/77 | |
| 9 | 59414 | | 11 | AST (HYBRID) /PS | 8/78-7/79 | |
| 10* | 030004 | BL.KR | -ВСТ | ASB/PS | 5/77-5/78 | |
| 11* | 030047 | | 18 | ASB/PS | 6/77-6/78 | |
| 12* | 030032 | 38 | 11 | ASB/PS | 11/77-11/78 | BOD Data Only |
| 13 | 01205 | 88 | Ħ | ASB/PS | (1-12)/79 | |
| 14 | 01203 | ** | 89 | ASB/PS(ST) | 4/78-2/79 | |
| 15 | 20601 | ** | 11 | ASB/PS | (1-10)/79 | |

| | TABLE A3 | | TIONS PROVIDING OR VARIABILITY / | | • • • • • • • • • • • • • • • • • • • |
|----------|---------------------|------------------------|-------------------------------------|--------------------|---------------------------------------|
| | | (C | ont.) | | |
| Mill No. | ID No. ³ | Production Category | Treatment Process | Data Time Frame | Comment |
| 16* | 030027 | BL.KRFINE | AST | 1/77-1/78 | |
| 17* | 030046 | TI 11 | ASB/PS | 7/77-7/78 | |
| 18* | 030020 | n | ASB/QZ/LA | 12/77-11/78 | |
| 19A | 34411 | 11 11 | AST/HYBRID | (1-12)/78 | |
| 19B | | | " "/CAC | 10/79-1/81 | CAC in Separate Facilities |
| 20 | 59407 | 89 BS | AST | (1-9)/78 | BOD Data Only |
| 21 | 74603 | F3 59 | AST | 4/76-6/77 | |
| 22 | 74606 | ¥1 80 | ASB/PS | 8/77-7/78 | |
| 23* | 010019 | UNBL.KRLNBD | ASB | 9/77-10/78 | |
| 24 | 29902 | 38 88 | ASB/PS | 1/76-4/79 | |
| 25 | 35201 | ta 82 | NSB | (1-11)/79 | |
| 26 | 52801 | ¥F 9F | ASB/PS | 10/77-8/78 | |
| 27 | 58701 | ** ** | ASB | (1-12)/79 | |
| 28 | 58902 | ti II | ASB/PS | 1/76-2/77 | |
| 29 | 74005 | 17 II | ASB | 1/79-1/80 | |

| | TABLE A3 | | ATIONS PROVIDING E FOR VARIABILITY AN | | |
|-------------------------|---------------------|-----------------------|--|--------------------|---|
| | | (co) | nt.) | | |
| Mill No. | ID No. ³ | Productio Category | n Treatment Process | Data Time Frame | Comment |
| 30 | 74601 | UNBL.KR/L | NBD AST | 3/77-7/78 | |
| 31* | 010055 | UNBL.KR/C | P ASB/PS | 10/77-10/78 | |
| 32* | 010003 | 81 81 | ASB/QZ | 11/77-11/78 | |
| 33 | 34416 | W 11 | ASB/PS | 1/78-4/79 | |
| 34 | 58916 | 81 SI | ASB | (1-12)/77 | |
| 35 | 45001 | UNBL.KR/S | PEC. AST, PC | | AST-PULP MILL I PC-PAPER MILL S |
| 36* | 020017 | SEMI-CHEM | . ASB/PS | 7/76-7/77 | |
| 37* | 020002 | ¥¥ ¥¥ | ASB/PS | 10/77-10/78 | |
| 38 | 43202 | ta 11 | ASB/MECH. CLARIF./PS | (1-12)/78 | |
| 39 | 50202 | TV TV | AST/HYBRID | 1/78-12/80 | |
| 4 0 [*] | 015002 | UNBL.KR/SI CHEM. | EMI- ASB/INFIL. BASIN | 11/77-11/78 | |
| 41* | 015007 | 9 9 89 | AST | 12/77-12/78 | |
| 42A | 15506 | 90 83 | ASB/PS | 10/77-7/78 | INCLUDES INTERMITTENT DISCH. FROM PULP MILL SPILL CONTAINMENT BASIN |
| 42B | | | | | CONTINUOUS DISCHARGE |

FROM ASB

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| | TABLE A3 | MILL LOCATION REVIEWED FOR V | NS PROVIDING I VARIABILITY AN | | |
|-----------------|---------------------|---------------------------------|----------------------------------|--------------------|--|
| | | (cont.) | | | |
| Mill No. | ID No. ³ | Production Category | Treatment Process | Data Time Frame | Comment |
| 43 | 69004 | UNBL.KR/SEMI- CHEM. (cont'd) | ASB | (1-12)/77 | |
| 4 4 * | 046006 | SULFITE-DISS. | ASB | 7/78-7/79 | |
| 45 [*] | 046004 | 10 11 | AST | 12/77-7/78 | |
| 46 | 35401 | 80 83 | ASB | 5/78-6/79 | |
| 47* | 040017 | SULFITE- PAPER | AST | 8/77-9/78 | |
| 48* | 040013 | 11 | PC, BIO- TREAT, PS | | → PC-Paper Mill, Bio-Treat- Pulp Mill, PS-Combined Disch. |
| 49 [*] | 040011 | H | UN- IDENTIFIED BIO-TREAT | 8/77-8/78 | Several Months of Limited or No BOD Removal, No Analysis Conducted |
| 50* | 040019 | U | AST, PC | | AST-Pulp Mill PC - Paper Mill |
| 51 | 17412 | | ASB | (1-7)/78 | Limited Data, No Variability Analysis Conducted |
| 52 | 06505 | ** | ASB | (1-12)/77 | |
| 53* | 052007 | GNDWD-FINE | AST | 1/77-1/78 | |
| 54 * | 052004 | 97 92 | AST | 1/77-1/78 | |

| | TABLE A3 | MILL LOC REVIEWED | | | |
|-----------------|---------------------|------------------------|--------------------------|--------------------|---|
| | | ((| | | |
| Mill No. | ID No. ³ | Production Category | Treatment Process | Data Time Frame | Comment |
| 55* | 080054 | INTEGRATED- MISC. | ASB/PS | 7/77-7/78 | |
| 56* | 150014 | 89 | AST | 7/77-7/78 | Limited Data, No Variability Analysis Conducted |
| 57* | 054013 | 11 | ASB/PS | 9/77-10/78 | Limited Data, No Variability Analysis Conducted & |
| 58 [*] | 060001 | n | ASB/MECH. CLARIF./CAC | 7/77-7/78 | CAL in Secondary Clarifier |
| 59 [*] | 140014 | DEINK-TISS | AST | 12/76-12/77 | |
| 60* | 140015 | " | AST | 11/77-11/78 | |
| 61* | 140007 | DEINK-FINE | AST | 7/77-7/78 | 7/77 Data Not Included, Start-up = ? |
| 62* | 085004 | WSTPAP-TISS. | ASB | 10/77-10/78 | Limited Data, No Variability Analysis Conducted |
| 63* | 090014 | 17 11 | PC | 10/77-10/78 | |
| 64* | 100005 | et 11 | ASB/PS | 9/77-9/78 | Limited BOD Data |
| 65* | 110052 | WSTPAP-BD | UN- IDENTIFIED | 9/77-9/78 | Limited Data, No Variability Analysis Conducted |
| 66* | 110032 | W 11 | UN-IDENTIFIED | 11/77-11/78 | an 10 |

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| | TABLE | | LOCATIONS PROVID | | |
|----------|---------------------|------------------------|----------------------|--------------------|---|
| | | (| cont.) | | |
| Mill No. | ID No. ³ | Production Category | Treatment Process | Data Time Frame | Comment |
| 67* | 110087 | WSTPAP-BD (Cont'd) | PC | 8/77-8/78 | No Variability Analysis Conducted |
| 68* | 110020 | | ASB/DAF | 11/77-10/78 | Limited Data, No Variability Analysis Conducted |
| 69* | 110031 | 13 95 | ASB/PS | 10/77-10/78 | |
| 70* | 110043 | 11 11 | ASB/PS | 1/78-1/79 | Limited Data, No Variability 🌫 Analysis Conducted 🕠 |
| 71 | 13801 | 17 19 | ASB/PS | (1-9)/78 | 14 11 12 12 12 12 12 12 12 12 12 12 12 12 |
| 72 | 13802 | 98 88 | ASB/DAF | (1-8)/78 | |
| 73 | 17408 | TT 00 | ASB/TF/LA/PS | 3/77-2/78 | Limited BOD Data |
| 74 | 42902 | 82 99 | ASB | 3/77-1/78 | |
| 75* | 150011 | WSTPAP- MOLD.PROD. | ASB | 8/77-8/78 | Limited Data, No Variability Analysis Conducted |
| 76* | 150024 | ۳. | POTW | 12/77-12/78 | Discharge to Municipal System, No Analysis Conducted |
| 77* | 120021 | BLDG.PAP & ROOF FLT. | UNIDENTIFIED | 6/77-6/78 | No Analysis Conducted |

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| TABLE A3 | MILL LOCATI | ONS PROVIDING | G DATA |
|----------|--------------|---------------|----------|
| | REVIEWED FOR | VARIABILITY | ANALYSIS |

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| (Cont | |) |
|-------|--|---|
|-------|--|---|

| Mill No. | ID No. ³ | Production Category | Treatment Process | Data Time Frame | Comment |
|-----------------|---------------------|---------------------------|----------------------|--------------------|--|
| 78* | 080046 | NONINTFINE | ASB | 7/77-6/78 | |
| 79 [*] | 080007 | " " | ASB/QZ | 7/77-7/78 | Limited Data, No Variability Analysis Conducted |
| 80 | 28715 | 98 PP | ASB/QZ | (1-12)/79 | 11 11 11 |
| 81 | 31105 | 17 IF | ASB | 1/78-1/79 | |
| 82 | 48102 | 22 P2 | AST | 5/77-4/78 | ` ≯ |
| 83* | 090005 | NONINTTISS | ASB | 9/77-10/78 | 10 |
| 84 | 090022 | | PC | 9/77-9/78 | No Variability Analysis Conducted |
| 85 | 38004 | 11 11 | AST/PS | (1-12)/79 | Limited BOD Data |
| 86 | 105013 | NONINTLWT. | AST/PS | 10/77-9/7 | Limited Data, No Variability |
| 87* | 105051 | NONINTFILT & NON-WOVEN | PC | 6/77-6/78 | Analysis Conducted No Variability Analysis Conducted |
| 88* | 105055 | 77 7 7 | AST | 9/77-9/78 | Limited Data, No Variability Analysis Conducted |

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| | TABLE | | | CATIONS PROVID | | |
|----------|---------------------|------------------------|------|----------------------|--------------------|------------------------------|
| | | | | (Cont.) | | |
| 1ill No. | ID No. ³ | Production Category | | Treatment Process | Data Time Frame | Comment |
| 89* | 110021 | NONINTPA | PBD. | ASB/QZ | 8/77-8/78 | Limited Data, No Variability |
| 90* | 085001 | | н | ASB | 10/77-10/78 | Analysis Conducted |
| 91 | 10901 | " | H | ASB/QZ | 1/79-1/80 | Limited BOD Data |
| 92* | 105024 | NONINTMI | sc. | PC | 8/76-9/77 | No Analysis Conducted |
| 93* | 105067 | u | H | PC | 8/77-8/78 | 91 68 44 |
| 94* | 105068 | | 11 | NSB(ST) | 9/77-9/78 | Limited BOD Data |
| 95 | 42916 | " | ŧ | PC | 1/79-1/80 | No Analysis Conducted |
| 96 | 59201 | " | # | NSB (ST) | (1-12)/77 | Limited BOD Data |

A-11

2) Mill No. Indicated with Note: 1) ASB = Aerated Stabilization Basin an * is a "Verification Mill". AST = Activated Sludge Treatment Data from these Mills Reviewed AST (HYBRID) = Biotreatment Process Using 2 to for Variability and Presented 4 days Aeration Followed by Mechanical in EPA's. Development Document, Clarification for Separation and Return of EPA 440/1-80/025-b, (Proposed). Bio-mass to Aerated Basin NSB = Natural Stabilization Basin 3) Other ID Nos. are NCASI Code PS = Post Stabilization in a Separate Basin ST = Short Term (less than one day) Numbers. PC = Primary Clarification TF = Trickling Filter LA = Land Application QZ = Quiescent Zone at Effluent End of ASB DAF = Dissolved Air Floatation CAC = Chemically Assisted Clarification

TABLE A4EFFLUENT QUALITY FROM PULP AND PAPERINDUSTRY WASTEWATER TREATMENT SYSTEMS

| No. | Mill Category | Nominal Production | Water_Usage(KGAL/TON) | BOI | D _s (lbs/Ton) | | TSS | 6 (1bs/To | <u>n</u>) |
|--------------------|------------------|-----------------------|-----------------------|------|--------------------------|------|------|-----------|------------|
| | | (TPD) | (AA) | | (MA30CD) ² | | (AA) | (MA30CD) | (MD) |
| 1 ^{*4, 5} | BL.KR,-DI | SS. 975 | 34.4 | 37.3 | 81.2 | 215 | 55.3 | 110 | 532 |
| 2/1 | | 1100 | 53.5 | 8.2 | 11.9 | 21.8 | 12.5 | 17.4 | 37.1 |
| 2/2 | | 1100 | 48.4 | 6.3 | 12.3 | 22.0 | 9.5 | 17.2 | 43.1 |
| 2/3 | • • | 1150 | 46.8 | 7.4 | 9.8 | 13.3 | 10.8 | 15.3 | 32.8 |
| 2/4 | | 1200 | 44.6 | 7.6 | 8.9 | 22.3 | 12.3 | 16.1 | 28.6 |
| 2/5 | | 1175 | 48.3 | 7.9 | 10.7 | 20.0 | 13.4 | 21.0 | 55.8 |
| 2/(1-5 | 5) " " | 1150 | 48.3 | 7.5 | 12.3 | 21.8 | 11.8 | 21.0 | 55.8 |
| 3/1 | | 1100 | 32.9 | 24.8 | 40.7 | 161 | 45.5 | 64.1 | 284 |
| 3/2 | | 975 | 34.6 | 38.5 | 81.9 | 215 | 56.4 | 110 | 531 |
| 3/(1-2 | :) = = | 1050 | 33.8 | 34.6 | 81.9 | 215 | 51.0 | 51.0 | 531 |
| 4* | BL.KR-MKT | . 800 | 31.9 | 4.4 | 9.3 | 11.6 | 6.4 | 13.9 | 19.0 |
| <u>5*</u> | | 375 | 16.6 | 13.4 | 34.4 | 43.4 | 10.2 | 16.7 | 24.5 |
| <u>6</u> | | 1275 | 45.3 | 11.2 | 15.5 | 30.0 | 19.9 | 26.5 | 64.2 |
| 2 | | 475 | 37.2 | 15.1 | 26.2 | 42.1 | 43.6 | 63.3 | 89.6 |
| <u>8</u> | • • | 525 | 32.6 | 6.8 | 12.4 | 25.5 | 7.8 | 12.1 | 33.0 |
| 9 | | 725 | 30.2 | 4.5 | 7.8 | 23.4 | 14.8 | 55.9 | 180 |
| 10* | BL.KR-BCT | 1025 | 40.9 | 5.9 | 9.9 | 18.6 | 7.8 | 9.6 | 15.8 |
| <u>11*</u> | • • | 575 | 34.0 | 11.8 | 33.4 | 55.7 | 11.1 | 18.6 | 34.0 |
| 12* | • • | 975 | 39.6 | 5.4 | 9.7 | 15.5 | 12.8 | - | - |
| <u>13</u> | | 950 | 43.6 | 9.5 | 12.7 | 33.6 | 8.6 | 11.2 | 29.8 |
| 14 | | 325 | 43.2 | 5.0 | 10.0 | 12.8 | 7.8 | 15.0 | 28.3 |
| <u>15</u> | | 1350 | 37.6 | 9.0 | 15.6 | 19.6 | 4.8 | 9.6 | 22.8 |
| <u>16</u> * | BL.KR-FINE | e 650 | 20.5 | 1.5 | 2.2 | 6.3 | 4.0 | 8.6 | 23.4 |
| 17* | • • | 875 | 30.4 | 4.3 | 9.1 | 12.7 | 7.2 | 19.8 | 31.6 |
| <u>18*</u> | • • | 500 | 23.6 | 2.1 | 3.2 | 5.0 | 4.7 | 6.1 | 13.2 |
| <u>19a</u> | | 725 | 22.8 | 3.5 | 8.6 | 11.2 | 17.5 | 39.3 | 74.4 |
| <u>19B</u> | | 600 | 23.1 | 2.6 | 5.9 | 15.3 | 7.3 | 13.4 | 22.8 |
| 20 | N N | 500 | 33.6 | 6.7 | 10.9 | 87.3 | 21.8 | - | - |
| 21 | | 1150 | 17.8 | 9.8 | 13.9 | 17.3 | 21.2 | 31.3 | 55.4 |
| 22 | • • | 400 | 52.5 | 12.9 | 22.4 | 31.0 | 11.2 | 19.9 | 27.1 |
| 23* | UNBL.KR/LM | NBD 1125 | 12.2 | 2.6 | 4.3 | 6.7 | 5.4 | 6.7 | 11.7 |
| 24/1 | • • | 625 | 7.5 | 3.4 | 7.5 | 13.8 | 10.4 | 33.6 | 66.5 |
| 24/2 | | 650 | 8.3 | 4.7 | 9.3 | 12.6 | 6.7 | 9.6 | 13.7 |
| 24/3 | H 9 | 650 | 8.0 | 3.7 | 6.1 | 7.7 | 6.5 | 9.9 | 22.0 |
| 24/(1- | 3)" " | 650 | 7.9 | 3,9 | 9.3 | 12.6 | 7.8 | 33.6 | 66.5 |

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EFFLUENT QUALITY FROM PULP AND PAPER TABLE A4 INDUSTRY WASTEWATER TREATMENT SYSTEMS (Cont'd)

| No. | Mill Category | Nominal Production | Water_Usage(KGAL/TON) | BOI | Oc(lbs/Ton |) | TSS | (lbs/Ton | 2 |
|------------|----------------------|-----------------------|------------------------------|-------------------|-----------------------|-------------------|------|----------|---------|
| | | (TPD) | (AA) | (AA) ¹ | (MA30CD) ² | (MD) ³ | (AA) | (MA30CD) | (MD) |
| 25 | UNBL.KR/LNBD. | 550 | 11.6 | 1.4 | 2.8 | 6.0 | 1.1 | 2.2 | 5.2 |
| 26 | H H | 950 | 12.1 | 2.1 | 2.9 | 5.3 | 4.0 | 4.6 | 8.1 |
| 27 | 80 PÌ | 1200 | 28.2 | 4.2 | 8.8 | 15.0 | 10.5 | 20.1 | 31.8 |
| 28 | • • | 1525 | 14.8 | 3.6 | 6.5 | 12.0 | 5.1 | 8.9 | 12.6 |
| <u>29</u> | * * | 800 | 10.9 | 3.8 | 9.3 | 12.8 | 6.6 | 9.6 | 21.9 |
| <u>30</u> | ** ** | 1800 | 14.2 | 2.3 | 5.1 | 14.0 | 10.2 | 11.2 | 44.5 |
| <u>31*</u> | UNBL.KR/CP | 775 | 12.1 | 5.6 | 9.1 | 12.0 | 7.2 | 10.0 | 13.0 |
| <u>32*</u> | • • | 300 | 12.4 | 4.5 | 7.5 | 16.1 | 8.3 | 10.9 | 21.3 |
| <u>33</u> | • • | 675 | 13.9 | 7.3 | 12.8 | 17.6 | 12.3 | 26.9 | 30.3 |
| <u>34</u> | • • | 1250 | 13.6 | 4.5 | 7.0 | 16.4 | 11.8 | 18.8 | 22.2 |
| <u>35</u> | UNBL.KR/SPEC, PAP | 250 | 50.4 | 6,9 | 9.1 | 21.0 | 13.8 | 17.8 | 45.1 |
| 36* | SEMI-CHEM. | 600 | 7.1 | 4.9 | 15.4 | 20.2 | 8.3 | 32.7 | 51.3 |
| 37* | n n | 350 | 6.1 | 5.6 | 15.2 | 21.2 | 4.7 | 8.9 | 11.1 |
| 38 | | 325 | 2.0 | 7.2 | 16.1 | 26.8 | 7.0 | 10.9 | 17.7 |
| 39/1 | | 625 | 9.6 | 1.4 | 4.0 | 8.2 | 4.9 | 11.7 | 17.7 |
| 39/2 | . . | 650 | 9.6 | 0.8 | 1.2 | 2.2 | 3.0 | 4.7 | 5.9 |
| 39/3 | | 650 | 11.3 | 0.7 | 1.8 | 2.2 | 3.0 | 5.6 | 9.9 |
| 39/(1 | -3)" " | 650 | 10.2 | 1.0 | 4.0 | 8.2 | 3.6 | 11.7 | 17.7 |
| 40* | UNBL.KR/SEMI | | | | | | | | |
| | CHEM. | 875 | 9.5 | 4.3 | 9.3 | 12.4 | 8.8 | 14.0 | 21.4 |
| 41* | 91 99 | 1800 | 11.7 | 4.5 | 9.5 | 36.1 | 7.7 | 12.7 | 39.8 |
| 42A | • • | 1300 | 9.5 | 4.7 | 20.4 | 114. | 3.4 | 16.6 | 79.8 |
| <u>42B</u> | • • | 1300 | 7.8 | 1.2 | 3.7 | 6.3 | 0.7 | 1.7 | 2.1 |
| <u>43</u> | H 11 | 2475 | 13.4 | 8.1 | 12.3 | 19.6 | 11.7 | 19.1 | 28.9 |
| 44* | SULFITE-DISS | 450 | 36.4 | 55.0 | 79.4 | 106. | 36.1 | 60.7 | 101. |
| 45* | * * | 625 | 39.9 | 33.3 | 44.7 | 110. | 145. | 174. | 355. |
| 46 | ¥ + | 450 | 35.2 | 51.8 | 84.0 | 122. | 33.1 | 64.9 | 98.4 |
| 47* | SULFITE-PAPE | R 525 | 21.1 | 9.1 | 15.2 | 30.0 | 18.7 | 26.0 | 67.5 |
| <u>48*</u> | | 350 | 22.6 | 30.2 | 46.5 | 84.1 | 16.5 | 29.2 | 44.2 |
| 49* | | Data no | t used - treatment system st | art-up | | | | | |
| <u>50*</u> | | 375 | 24.9 | 8.0 | 13.6 | 40.7 | 8.0 | | 38.2 |
| 51 | * * | 75 | 34.2 | 27.8 | Limited | d Data | 25.0 | | ed Data |
| <u>52</u> | | 250 | 60.0 | 21.7 | | 67.0 | 29.3 | | |
| <u>53*</u> | GRNDWD-FINE | 225 | 21.6 | 2.1 | 4.8 | 13.7 | 6.0 | | 24.3 |
| 54* | | 500 | 14.2 | 6.0 | 10.9 | 19.1 | 6.6 | 13.6 | 31.5 |

TABLE A4EFFLUENT QUALITY FROM PULP AND PAPER
INDUSTRY WASTEWATER TREATMENT SYSTEMS
(Cont'd)

| <u>No.</u> | Mill Category | Nominal Production | Water_Usage(KGAL/TON) | во | D ₅ (lbs/Ton) | TSS | (lbs/Ton) |
|--------------|----------------------------|-----------------------|-----------------------|-------------------|---|------|-------------------|
| | | (TPD) | (AA) | (AA) ¹ | (MA30CD) ² (MD) ³ | (AA) | (MA30CD) (MD) |
| <u>55</u> | INT-MISC. | 50 | 7.7 | 4.5 | 9.8 13.1 | 3.6 | 6.7 17.5 |
| 56 | | 75 | 12.4 | 2.6 | Limited Data | 1.6 | Limited Data |
| 57 | P\$ \$\$ | 50 | 40.5 | 7.4 | Limited Data | 1.7 | Limited Data |
| 58 | INT-MISC. | 75 | 22.7 | 2.7 | 5.7 10.8 | 1.9 | 2.9 5.1 |
| <u>59*</u> | DEINK-TISS | 850 | 21.5 | 6.9 | 10.1 27.0 | 13.6 | 24.5 89.4 |
| <u>60*</u> | | 50 | 19.3 | 5.0 | 9.4 19.1 | 7.1 | 11.0 24.2 |
| 61* | DEINK-FINE | 375 | 11.1 | 12.4 | 42.1 65.3 | 13.0 | 30.7 172. |
| 62* | WSTEPAPER- TISS | 50 | 14.7 | 5,2 | Limited Data | 4.7 | Limited Data |
| 63* | | 50 | 22.4 | 8.7 | | 8.7 | rt 17 |
| 64* | | 50 | 5.4 | 2.8 | M N | 2.4 | 5.6 9.9 |
| 65* | WSTEPAPER- BD | 100 | 52.4 | 1.4 | Limited Data | 1.5 | Limited Data |
| 66* | • | 75 | 8.9 | 2.5 | ** ** | 3.5 | b0 B 5 |
| 67* | • | 450 | 0.7 | 20.5 | P/C System | 0.5 | P/C System |
| 68* | • | 75 | 11.2 | 1.9 | Limited Data | 3.4 | Limited Data |
| <u>69*</u> | - | 150 | 1.9 | 0.3 | 0.6 0.8 | 0.4 | 0.7 0.9 |
| 70* | - | 150 | 3.2 | 1.5 | Limited Data | 2.1 | Limited Data |
| 71 | • | 75 | 7.4 | 1.5 | • • | 2.0 | 19 19 |
| 72 | m | 75 | 10.9 | 1.9 | M N | 3.4 | e 11 |
| 73 | * | 175 | 1.6 | 1.6 | • • | 1.6 | 5.7 11.9 |
| <u>74</u> | • | 200 | 2.7 | 1.9 | 3.5 4.9 | 1.5 | 2.4 4.9 |
| <u>75</u> * | WSTEPAPER-MO PROD. | 1LD 75 | 17.2 | 4.5 | Limited Data | 3.1 | Limited Data |
| 76* | w 17 | 100 | 19.0 | 11.8 | Discharge to | 32.1 | POTW |
| 77* | BLDG PAP. & | 175 | 0.1 | 2.6 | Limited Data | 0.2 | Limited Data |
| <u>78*</u> | NONINT-FINE | 550 | 11.6 | 4.4 | 7.9 10.4 | 6.0 | 10.2 15.4 |
| 79* | | 175 | 14.9 | 3.5 | Limited Data | 3.2 | Limited Data |
| 80 | n n | 175 | 16.4 | 3.0 | 81 9 1 | 4.4 | |
| <u>81</u> | M 11 | 525 | 12.6 | 5.2 | 8.4 11.8 | 5.1 | 7.4 10.5 |
| <u>82</u> | | 200 | 12.2 | 4.1 | 5.9 18.2 | 4.7 | 5.7 11.2 |
| 83* | NONINT-TISS. | 40 | 5.5 | 0.8 | 1.7 2.1 | .1.1 | 0.9 2.7 |
| 84 | T T | 175 | 15.6 | 6.5 | Limited Data | 4.9 | Limited Data |
| 85 | | 150 | 22.8 | 2.7 | * • | 2.9 | 6.2 14.5 |
| `86 * | NON INT-LTWT | 10 | 112. | 21.4 | | 24.3 | Limited Data |
| 87* | NONINT-FILT & NON WOVEN | 10 | 42.3 | 2.7 | P/C System | 4.5 | P/C System |

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TABLE A4 EFFLUENT QUALITY FROM PULP AND PAPER INDUSTRY WASTEWATER TREATMENT SYSTEMS (Cont'd)

| No. | Mill Category | Nominal Production | Water Usage (KGAL/TON) | BOD ₅ (lbs/Ton) | TS | S (lbs/Ton) |
|------------|----------------------------|-----------------------|------------------------|--------------------------------|------|---------------|
| | | (TPD) | (AA) | $(AA)^1$ $(MA30CD)^2$ $(MD)^3$ | (AA) | (MA30CD) (MD) |
| 88* | NONINT-FILT & NON WOVEN | 30 | 95.8 | 3.4 Limited Data | 7.9 | Limited Data |
| 89* | NONINT-PAPBD | 75 | 14.4 | 2.6 " | 4.3 | |
| 90* | n _ n | 75 | 6.1 | 1.7 • • | 0.2 | • • |
| 91 | | 75 | 13.3 | 3.6 " " | 5.4 | 14.2 26.6 |
| <u>92*</u> | NONINT- MISC. | 200 | 23.6 | 1.4 P/C System | 2.1 | P/C System |
| 93* | - | 40 | 35.8 | 3.5 P/C System | 1.6 | P/C System |
| <u>94*</u> | * | 75 | 20.2 | 4.3 Limited Data | 2.1 | 4.2 8.3 |
| 9 5 | * | 40 | 33.6 | 5.0 P/C System | 1.6 | P/C System |
| <u>96</u> | W | 75 | 18.5 | 3.9 Limited Data | 1.5 | 2.0 6.4 |

Notes: 1) AA = Annual or Long Term Average.

- 2) MA30CD Maximum Average for Thirty Consecutive Days. The MA30CD value for BOD, and TSS is the actual MA30CD value in pounds per day divided by the average thirty day production for the same period.
- 3) MD = Maximum Day. The MD value is the MD value in pounds per day divided by the production that occurred on that day.
- 4) Mill numbers indentified with an * are the "verification mills" data provided by the EC Jordan Co. and used in the development of effluent variability factors.
- 5) Mill numbers which are underlined were used in variability analysis.

TABLE A5

ANALYSIS OF PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED EFFLUENTS FOR SELECTED DISTRIBUTION FUNCTIONS DAILY EFFLUENT QUALITY (KLBS/DAY)

| | Prod. | | | BOD ₅ | | | | TSS | |
|----------------|-------------------|------|----|----------------------|------------------|------|--------------|---------|-----|
| Mill No. | Category | OBS. | Nl | $\frac{BOD_5}{LN^2}$ | SLN ³ | OBS | <u>N</u> | LN | SLN |
| 1 | BK-DISS | 363 | - | - | ¥4 | 374 | - | - | - |
| 2-1 | 17 | 352 | - | - | Y | 354 | - | - | Y |
| 2-2 | n H | 356 | - | - | - | 356 | - | Y | - |
| 2-3 | н н | 354 | - | Y | - | 355 | - | - | Y |
| 2-4 | ** ** | 355 | | Y | - | 356 | - | - | Y |
| 2-5 | 11 11 | 354 | - | Y | - | 357 | - | - | Y |
| 2/(1-5) | tt tt | 1771 | - | - | - | 1778 | - | - | - |
| 3-1 | | 300 | - | - | Y | 300 | - | Y | - |
| 3-2 | 14 PI | 338 | - | - | Y | 350 | - | - | - |
| 3/(1-2) | 11 IT | 638 | - | - | Y | 650 | - | Y | - |
| 4 | BK-MKT | 178 | | - | Y | 176 | - | - | Y |
| 5 | 94 1 4 | 344 | - | - | Y | 356 | - | - | - |
| 6 | 11 et | 361 | - | - | Y | 361 | - | - | - |
| 7 | 11 II | 322 | - | - | - | 328 | - | - | - |
| 8 | n n | 277 | - | - | - | 312 | - | - | Y |
| 9 | n n | 337 | - | Y | - | 337 | - | _ | - |
| 10 | BK-BCT | 385 | - | - | Y | 387 | Y | - | |
| 11 | 99 99 | 368 | - | | - | 373 | - | - | - |
| 12 | 17 II | 341 | - | Y | - | 32 | Limited | TSS Da | |
| 13 | | 350 | - | - | Y | 352 | - | | Y |
| 14 | ri et | 255 | - | - | - | 141 | - | - | Y |
| 15 | PT H | 129 | - | Y | - | 129 | - | - | Y |
| 16 | BK-FINE | 376 | - | - | - | 381 | - | Y | - |
| 17 | 44 et | 373 | - | - | Y | 379 | | - | - |
| 18 | PT +0 | 356 | - | - | - | 356 | - | - | Y |
| 19A | 19 91 19 91 | 145 | - | - | · _ | 273 | - | Y | - |
| 19B | 79 97 97 97 | 196 | - | Y | - v | 417 | - Limitod | - | Y |
| 20 | | 265 | | - | Y | 89 | Limited | 155 Dat | |
| 21 | 67 85 | 434 | Y | - | - | 446 | - | - | Y |
| 22 | M M | 242 | - | - | Y | 363 | - | - | Y |
| 23 | UBK-LNBD | 175 | - | Y | - | 172 | - | Y | - |
| 24-1 | 99 89 | 159 | - | - | Y | 160 | - | - | Y |
| 2 4 – 2 | P1 P1 | 164 | - | Y | - | 164 | - | Y | - |
| 2 4 -3 | 14 st | 177 | Y | - | - | 177 | - | - | - |
| 24/(1-3) | N N | 500 | - | - | Y | 501 | - | - | - |
| 25 | 99 1 4 | 292 | - | - | - | 286 | - | Y | - |
| 26 | 11 11 | 273 | _ | - | - | 310 | - | Y | |
| 27 | 19 19 | 333 | _ | Y | - | 341 | - | - | - |
| | | | | | V | | | | _ |
| 28 | UBK-LNBD | 385 | | - | Y | 399 | - | - | - |
| 29 | 12 14 | 166 | - | Y | - | 166 | - | Y | - |

TABLE A5

ANALYSIS OF PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED EFFLUENTS FOR SELECTED DISTRIBUTION FUNCTIONS DAILY EFFLUENT QUALITY (KLBS/DAY)

| | | | | BOD ₅ | | | | TSS | |
|----------|-------------------|------|----------------------|------------------|---------------------|------|------|-----------|--------|
| Mill No. | Prod. Category | OBS. | <u>N¹</u> | | SLN ³ | OBS | N | <u>LN</u> | SLN |
| 30 | UBK-LNBD | 306 | - | ¥ | - | 311 | - | Y | - |
| 31 | UBK-CP | 218 | - | Y | - | 218 | ¥ | - | - |
| 32 | •• •• | 257 | | - | - | 239 | - | - | Y |
| 33 | M | 315 | - | Y | - | 315 | - | - | - |
| 34 | * * | 354 | - | - | - | 354 | - | - | - |
| 35 | UBK-SPEC. PAP. | 355 | - | Y | - | 355 | - | - | - |
| 36 | SEMI-CHEM | 370 | - | - | - | 367 | - | - | - |
| 37 | • • | 362 | - | - | - | 369 | - | - | Y |
| 38 | 99 93 | 310 | - | - | Y | 319 | - | - | . – |
| 39-1 | 11 II | 333 | - | - | - | 333 | - | - | - |
| 39-2 | 97 N | 359 | - | - | Y | 360 | - | - | - |
| 39-3 | ** ** | 339 | - | - | - | 341 | - | - | - |
| 39/(1-3) | я я | 1031 | - | - | - | 1034 | - | - | - |
| 40 | UBK/SEM- Chem. | 159 | - | - | - | 159 | - | Y | · 🕳 |
| 41 | н н | 347 | - | - | - | 347 | - | - | - |
| 42B | n n | 298 | - | - | - | 298 | - | - | - |
| 43 | 74 FT | 347 | - | - | - | 345 | - | - | - |
| 44 | SULF-DISS | 376 | Y | - | - | 376 | - | - | Y |
| 45 | PT 93 | 221 | - | - | Y | 223 | - | - | Y |
| 46 | n n | 422 | - | - | - | 421 | - | - | Y |
| 47 | SULF-PAP | 421 | - | - | - | 421 | - | Y | - |
| 48 | 99 BB | 370 | - | - | - | 370 | - | - | - |
| 50 | n n | 159 | - | Y | - | 384 | - | Y | - |
| 51 | ** ** | 89 | Lim | ited BO | D ₅ Data | 33 | Limi | ted TSS | 5 Data |
| 52 | et 13 | 244 | - | - | - | 299 | - | Y | - |
| 53 | GNDWD-FINE | 384 | - | - | | 387 | - | - | - |
| 54 | ts to | 354 | - | - | Y | 353 | - | - | - |
| 55 | INT-MISC. | 317 | - | - | - | 317 | - | - | - |
| 58 | n n | 381 | - | - | Y | 379 | - | - | Y |
| 59 | DEINK-TISS. | 388 | | Y | - | 391 | - | - | - |
| 60 | 11 H | 369 | | - | - | 369 | - | - | - |
| 61 | DEINK-FINE | 357 | - | - | - | 361 | - | - | - |

TABLE A5ANALYSIS OF PULP AND PAPER INDUSTRY
BIOLOGICALLY TREATED EFFLUENTS
FOR SELECTED DISTRIBUTION FUNCTIONS
DAILY EFFLUENT QUALITY (KLBS/DAY)
(Cont'd)

| | Prod. | | BOD5 | | TSS |
|----------|----------------|------|--|--------------|--------------|
| Mill No. | Category | OBS. | $\underline{N^1}$ $\underline{LN^2}$ $\underline{SLN^3}$ | OBS <u>N</u> | LN SLN |
| 66 | WSTPAP-TISS | 105 | Limited BOD ₅ Data | 106 Limit | ed TSS Data |
| 69 | • • | 151 | | 151 - | ¥ - |
| 73 | ** ** | 94 | Limited BOD ₅ Data | 249 - | у – |
| 74 | M N | 283 | - Y - | 293 - | ¥ - |
| 78 | NONINT-FINE | 350 | Y | 350 - | ч – |
| 81 | w n | 382 | - Y - | 382 - | |
| 82 | * * | 347 | | 348 - | У – |
| 83 | NONINT-TISS | 144 | | 192 - | - Y |
| 85 | n 1 | 91 | Limited BOD ₅ Data | 336 - | ¥ - |
| 89 | NONINT-PAPBD | 87 | Limited BOD ₅ Data | 95 Limit | ed TSS Data |
| 90 | n | 100 | Limited BOD ₅ Data | 100 Limit | ted TSS Data |
| 91 | n n | 101 | Limited BOD ₅ Data | 170 - | ч – |
| 94 | NONINT-MISC. | 83 | Limited BOD ₅ Data | 271 - | Y - |
| 96 | | 76 | Limited BOD ₅ Data | 223 - | - ¥ |

- NOTE: 1) N = Normal Distribution
 - 2) LN = Log Normal Distribution
 - 3)SLN = Shifted Log Normal Distribution
 - 4) Y = Indicates that the data adhere to the distribution cited at the top of the column.

ESTIMATE OF VARIABILITY IN PULP AND PAPER TABLE A6 INDUSTRY BIOLOGICALLY TREATED EFFLUENTS MAXIMUM DAY - BOD₅ (KLBS/DAY)

| Mill No. | % - Tile | Non Parametric Estimate at 50% TL 5% TL | Distrib. Function Estimate Value Basis | Max. Daily Value | Long Term Avg. | Variat 50% TL | bility ¹ - 5 <u>% TL</u> | Based | Upon M.D.V. |
|-------------|-------------------------------|---|--|------------------------|----------------------|---------------------------|--|------------------------------|-------------------|
| 1 | 99 99.7 99.9 99.95 | 150.1 190.7 190.7 > 198.2 | 146.9 SLN 194.3 * 245.1 * 274.4 * | 198.2 | 36.57 | 4.10 5.21 - | 5.21 >5.42 - | 4.02 5.31 6.70 7.50 | 5.42 |
| 2-1 | 99 99.7 99.9 99.95 | 20.87 25.50 25.50 > 27.83 | 20.19 SLN 23.02 " 25.68 " 27.09 " | 27.83 | 8.951 | 2.33 2.85 _ | 2.85 >3.11 - | 2.26 2.57 2.87 3.03 | 3.11 |
| 2-2 | 99 99.7 | 22.06 22.97 22.97 > 23.38 | No FIT | 23.38 | 6.974 | 3.16 3.29 | 3.29 ≻3.35 | - | 3.35 |
| 2-3 | 99 99.7 99.9 99.95 | 15.19 15.69 15.69 > 16.68 | 15.17 LN 16.90 " 18.50 " | 16.68 | 8.602 | 1.76 1.82 - | 1.82 >1.94 | 1.76 1.96 2.15 | 1.94 |
| 2-4 | 99 99.7 99.9 99.95 | 16.94 17.68 17.68 > 17.79 | 16.56 LN 18.60 " 20.49 " 21.47 " | 17.78 | 9.032 | 1.88 1.95 _ | 1.95 >1.97 - | 1.83 2.06 2.27 2.38 |] ⁻ 06 |
| 2-5 | 99 99.7 99.9 99.95 | 20.53 23.05 23.05 > 23.39 | 19.58 LN 22.61 " 25.49 " 27.02 " | 23.39 | 9.342 | 2.12 2.47 _ | 2.47 >2.50 _ | 2.10 2.42 2.73 2.89 | 2.50 |
| 2/(1-5 | 5)99 99.7 99.9 99.95 | 18.71 20.83 23.05 23.39 23.39 > 27.83 | NO FIT | 27.83 | 8.578 | 2.18 2.69 2.73 | 2.43 2.73 > 3.24 | - - - - | 3.24 |
| 3-1 | 99 99.7 99.9 99.95 | 100.1 116.7 116.7 > 174.9 | 117.2 SLN 157.3 " 201.0 " 226.3 " | 174.9 | 27.26 | 3.67 4.28 _ _ | 4.28 >6.42 - | 4.30 5.77 7.37 8.30 | 6.42 |
| 3-2 | 99 99.7 99.9 99.95 | 150.1 190.5 190.5 > 198.1 | 152.0 SLN 201.0 " 253.7 " 284.0 " | 198.1 | 37.50 | 4. 00 5.08 | 5.08 >5.28 | 4.05 5.36 6.77 7.57 | 5.28 |
| 3/(1-2 | 2)99 99.7 99.9 99.95 | 131.0 150.1 174.9 > 198.1 198.1 > 198.1 | 139.0 SLN 185.9 " 236.9 " 266.5 " | 198.1 | 32.69 | 4.01 5.35 6.06 - | 4.59 > 6.06 > 6.06 - | 4.25 5.69 7.25 8.15 | 6.06 |
| 4 | 99 99.7 99.9 99.95 | B.564 > 9.641 9.641 > 9.641 | 12.00 SLN 13.61 " 15.10 " 15.88 " | 9.64 | 3.56 | 2.40 2.70 - | > 2.70 > 2.70 - - | 3.37 3.82 4.24 4.45 | 2.70 |
| 5 | 99 99.7 99.9 99.95 | 15.13 16.52 16.11 > 16.52 | 16.96 SLN 22.28 " 27.96 " 31.22 " | 16.52 | 5.02 | 3.01 3.21 - | 3.29 > 3.29 - - | 3.38 4.44 5.57 6.22 | 3.29 |
| 6 | 99 99.7 99.9 99.95 | 31.38 31.85 31.85 > 32.23 | 43.26 SLN 46.97 " 50.30 " 52.00 " | 32.23 | 14.20 | 2.21 2.24 _ | 2.24 > 2.27 - - | 3.05 3.31 3.54 3.66 | 2.27 |
| 7 | 99 99.7 99.9 99.95 | 20.96 22.68 22.68 25.67 | NO FIT | 25.67 | 7.28 | 2.88 3.12 - | 3.12 > 3.53 - | - - - | 3.53 |
| 8 | 99 99.7 99.9 99.95 | 11.30 13.08 12.66 >13.08 | NO FIT | 13.08 | 3.52 | 3.21 3.60 - | 3.72 >3.72 _ | | 3.72 |
| 9 | 99 99.7 | 13.26 17.66 17.66 >20.59 | 12.29 LN 16.19 " | 20.59 | 3.29 | 4.03 5.37 | 5.37 >6.26 | 3.74 4.92 | 6.26 |

| | | Non Parametric | Distrib. Function | Max. | Long | | 1 | | |
|--------------------|-----------------------------|--|--|----------------|--------------|------------------------|---------------------------------|------------------------------|----------------|
| Mill <u>No.</u> | % - Tile | Estimate at 50% TL 5% TL | <u>Estimate</u> Value Basis | Daily Value | Term Avg. | Variat 50% TL | 5 <u>% TL</u> | D.F. | Upon M.D.V. |
| 10 | 99 99.7 99.9 99.95 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 16.75 SLN 18.98 " 21.07 " 22.17 " | 17.75 | 6.04 | 2.14 2.38 _ | 2.38 > 2.94 _ | 2.77 3.14 3.49 3.67 | 2.94 |
| 11 | 99 99.7 99.9 99.95 | 28.20 30.02 30.02 31.02 | NO FIT | 31.02 | 6.71 | 4.20 4.47 _ _ | 4.47 > 4.62 - | - - - | 4.62 |
| 12 | 99 99.7 99.9 99.95 | 11.68 12.52 12.52 > 12.56 | 13.72 LN 16.58 H 19.41 H 20.95 H | 12.56 | 5.31 | 2.20 2.35 - | 2.35 > 2.36 | 2.58 3.12 3.65 3.95 | 2.36 |
| 13 | 99 99.7 99.9 99.95 | 19.65 19.97 19.97 > 23.94 | 26.95 SLN 29.98 " 32.76 " 34.20 " | 23.94 | 9.03 | 2.18 2.21 - | 2.21 > 2.65 - | 2.98 3.32 3.63 3.79 | 2.65 |
| 14 | 99 99.7 99.9 99.95 | 4.07 4.27 4.13 > 4.27 | No FIT | 4.27 | 1.65 | 2.47 2.50 | 2.58 > 2.58 _ _ | - - - | 2.58 |
| 15 | 99 99.7 99.9 99.95 | 24.35 > 26.95 26.95 > 26.95 | 27.52 LN 32.34 " 37.01 " 39.51 " | 26.95 | 12.10 | 2.01 2.23 - | > 2.23 > 2.23 - - | 2.27 2.67 3.06 3.27 | 2.23 |
| 16 | 99 99.7 99.9 99.95 | 2.33 2.79 2.79 > 3.61 | No FIT | 3.61 | 0.99 | 2.35 2.82 - - | 2.82 > 3.65 _ _ | - | 3.65 |
| 17 | 99 99.7 99.9 99.95 | 9.88 12.73 12.73 > 13.16 | 11.69 SLN 15.19 " 18.90 " 21.06 " | 13.16 | 3.82 | 2.58 3.33 - | 3.33 >.3.45 | 3.06 3.98 4.95 5.51 | 3.45 |
| 18 | 99 99.7 99.9 99.95 | 2.70 2.79 2.79 > 2.82 | No FIT | 2.82 | 1.04 | 2.60 2.68 - | 2.68 > 2.71 - - | - - - | 2.71 |
| 19A | 99 99.7 99.9 99.95 | 8.51 > 8.86 8.86 > 8.86 | No FIT | 8.86 | 2.58 | 3.30 3.43 _ | > 3.43 > 3.43 - - | - - - | 3.43 |
| 19B | 99 99.7 99.9 99.95 | 6.31 > 9.19 9.19 > 9.19 | 6.96 LN 9.59 " 12.53 " 14.27 " | 9.19 | 1.57 | 4.02 5.85 - | > 5.85 > 5.85 - - | - - - | 5.85 |
| 20 | 99 99.7 99:95 | 17.44 34.29 34.29 > 34.29 = = | 14.59 SLN 21.18 " 28.88 " 33.58 " | 34.29 | 3.27 | 5.33 10.49 _ | 10.49 > 10.49 - - 1 | | 10.49 |
| 21 | 99 99.7 99.9 99.95 | 19.63 22.02 22.02 > 22.46 | 19.88 N 21.45 " 22.76 " 23.39 " | 22.46 | 11.20 | 1.75 1.97 _ | | | 2.01 |
| 22 | 99 99.7 99.9 99.95 | 11.63 >12.73 11.90 12.73 | 15.84 SLN 17.57 " 19.16 " 19.97 " | 12.73 | 5.31 | 2.19 2.24 - - | | | 2.40 |

.

(Cont'd)

| Mill No. | % - Tile | Non Parametric Estimate at 50% TL 5% TL | Distrib. Funct Estimate Value Basis | Daily | Long Term Avg. | Variat 50% TL | bility ¹ - 5 <u>% TL</u> | Based D.F. | Upon M.D.V. |
|---------------|-----------------------------|---|--|-------|----------------------|----------------------|--|------------------------------|----------------|
| 23 | 99 99.7 99.9 99.95 | 7.68 > 8.89 8.89 > 8.89 | 7.18 LN 8.59 " 9.97 " 10.72 " | 8.89 | 2.93 | 2.62 3.03 | > 3.03 > 3.03 - | 2.45 2.93 3.40 3.66 | 3.03 |
| 2 4- 1 | 99 99.7 99.9 99.95 | >7.30 7.74 >7.74 7.74 | 6.53 SLN 7.55 " 8.52 " 9.04 " | 7.74 | 2.13 | 3.42 3.63 _ | > 3.63 > 3.63 _ _ | 3.07 3.54 4.00 4.24 | 3.63 |
| 24-2 | 99 99.7 99.9 99.95 | 6.98 > 8.87 8.87 > 8.87 | 7.79 LN 9.39 " 10.97 " 11.83 " | 8.87 | 3.04 | 2.30 2.92 _ | > 2.92 > 2.92 - - | 2.56 3.09 3.60 3.89 | 2.92 |
| 24-3 | 99 99.7 99.9 99.95 | 3.91 > 4.22 4.22 > 4.22 """" | 4.17 N 4.46 " 4.72 " 4.85 " | 4.22 | 2.39 | 1.63 1.77 _ | >1.77 >1.77 - | 1.74 1.87 1.97 2.02 | 1.77 |
| 24/(1-3) | 99 99.7 99.9 99.95 | 6.56 7.30 7.74 > 8.87 8.87 > 8.87 | 7.06 SLN 8.03 " 8.95 " 9.43 " | 8.87 | 2.52 | 2.60 3.07 3.52 | 2.90 >3.52 >3.52 | 2.80 3.19 3.51 3.74 | 3.52 |
| 25 | 99 99.7 99.9 99.95 | 1.92 3.50 2.05 > 3.50 | NO FIT | 3.50 | 0.80 | 2.40 2.56 _ | 4.38 > 4.38 - - | - - - | 4.38 |
| 26 | 99 99.7 99.9 99.95 | 4.16 5.40 4.60 > 5.40 | No FIT | 5.40 | 2.04 | 2.04 2.25 | 2.65 > 2.65 - - | | 2.65 |
| 27 | 99 99.7 99.9 99.95 | 13.03 15.64 15.64 > 16.38 | 14.86 LN 18.60 " 22.40 " 24.58 " | 16.38 | 4.86 | 2.68 | 3.22 > 3.37 - | 3.06 3.83 4.61 5.06 | 3.37 |
| 28 | 99 99.7 99.9 99.95 | 15.18 17.31 17.31 > 17.39 | 18.45 SLN 21.76 " 24.97 " 26.69 " | 17.39 | 5.44 | 2.79 3.18 _ | 3.18 > 3.19 _ | 3.39 4.00 4.59 4.91 | 3.19 |
| 29 | 99 99.7 99.9 99.95 | 11.09 > 11.09 11.09 > 11.09 | 8.33 LN 10.19 " 12.02 " 13.03 " | 11.09 | 3.09 | 3.59 3.59 _ | > 3.59 > 3.59 _ _ | 2.70 3.30 3.89 4.22 | 3.59 |
| 30 | 99 99.7 99.9 99.95 | 11.76 18.92 18.92 > 18.92 | 10.21 LN 12.25 " 14.25 " 15.34 " | 18.92 | 4.13 | 2.85 4.58 - | 4.58 >4.58 _ _ | 2.47 2.97 3.45 3.71 | 4.58 |
| 31 | 99 99.7 99.9 99.95 | 9.25 > 10.06 10.06 > 10.06 | 10.18 LN 12.04 " 13.86 " 14.84 " | 10.06 | 4.31 | 2.15 2.33 | > 2.33 > 2.33 | 2.36 2.79 3.22 3.44 | 2.33 |
| 32 | 99 99.7 99.9 99.95 | 4.11 4.81 4.20 > 4.81 | No FIT | 4.81 | 1.31 | 3.14 3.21 - | 3.67 > 3.67 _ _ | - - - | 3.67 |
| 33 | 99 99.7 99.9 99.95 | 9.05 10.06 10.06 > 11.09 | 11.56 LN 13.54 " 15.45 " 16.47 " | 11.09 | 5.16 | 1.75 1.95 - | 1.95 >2.15 - | 2.24 2.62 2.99 | 2.15 |

| Mill <u>No.</u> | % - Tile | Non Parametric Estimate at 50% TL 5% TL | Distrib Esti Value | . Function mate Basis | Max. Daily Value | Long Term Avg. | Variability ¹ -Based Upon 50% TL 5% TL D.F. M.D.V. |
|--------------------|-------------------------------------|--|--|-----------------------------|------------------------|----------------------|--|
| 34 | 99 99.7 9 9.9 99.95 | 18.51 20.68 20.68 > 21.30 | No | FIT | 21.30 | 5.71 | 3.58 4.01 - 4.13 4.01 > 4.13 - |
| 35 | 99 99.7 99.9 99.95 | $\begin{array}{cccc} 4.65 & 5.12 \\ 5.12 & > 5.43 \\ - & - \\ - & - \\ - & - \\ \end{array}$ | 4.28 5.09 5.87 6.29 | LN " | 5.43 | 1.71 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 36 | 99 99.7 99.9 99.95 | 10.94 13.18 13.18 > 13.51 | No | FIT | 13.51 | 2.97 | 3.68 4.44 - 4.55 4.44 > 4.55 - |
| 37 | 99 99.7 99.9 99.95 | 7.04 7.53 7.53 > 7.62 | NO | FIT | 7.62 | 1.85 | 3.81 4.07 - 4.12 4.07 4.12 - |
| 38 | 99 99.7 99.9 99.95 | 8.31 8.78 8.78 > 10.27 | 8.90 11.53 14.32 15.90 | SLN " " | 10.27 | 2.31 | 3.60 3.80 3.85 4.45 3.80 > 4.45 4.99 6.20 6.88 |
| 39-1 | 99 99.7 99.9 99.95 | 2.99 3.38 3.38 > 5.11 | No | FIT | 5.11 | 0 <u>.</u> 89 | 3.36 3.80 - 5.74 3.80 > 5.74 - |
| 39-2 | 99 99.7 99.9 99.95 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1.58 1.74 1.89 1.96 | SLN n n | 1.47 | 0.50 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 39-3 | 99 99.7 99.9 99.95 | 1.43 1.50 1.50 > 1.57 | No | FIT | 1.57 | 0.46 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 39/(1-3) | 99 99.7 99.9 99.95 | 2.57 2.89 2.99 3.38 3.38 > 5.11 | No | FIT | 5.11 | 0.61 | 4.21 4.74 - 8.38 4.90 5.54 - 5.54 > 8.38 - |
| 40 | 99 99.7 99.9 99.95 | 9.80 > 11.26 11.26 > 11.26 | No | FIT | 11.26 | 3.80 | 2.58 > 2.96 - 2.96 2.96 > 2.96 - |
| 41 | 99 99.7 99.9 99.95 | 34.68 51.83 51.83 > 52.67 | No | FIT | 52.67 | 8.06 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 4 2B | 99 99.7 99.9 99.95 | 5.51 6.11 5.95 > 6.11 | No | FIT | 6.11 | 1.52 | 3.63 4.02 - $4.023.91 > 4.02$ - |
| 43 | 99 99.7 99.9 99.95 | 38.11 43.23 43.23 > 46.67 | No | FIT | 46.67 | 19.9 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 44 | 99 99.7 99.9 99.95 | 46.42 53.55 53.55 , 55.11 | 46.7 3 50.70 54.00 55.60 | N M M | 55.11 | 24.80 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |

(Cont'd)

| Mill | 8 - | Non Parametric Estimate at | Distrib. Function | Max. Daily | Long Term | Variability ¹ | -Rased Upon |
|------------------|--------------------------------------|---|---|-----------------------|----------------------|---|-------------------------------|
| <u>No.</u> 45 | <u>Tile</u> 99 99.7 99.9 | 50% TL 5% TL 43.28 53.05 53.05 53.05 | Value <u>Pasis</u> 58.87 SLN 65.44 " 71.47 " | <u>Value</u> 53,05 | <u>Avg.</u> 20.50 | <u>50% TL</u> 5 <u>% TL</u> 2.11 2.5 2.59 2.5 | 9 2.87 2.59 9 3.19 3.49 |
| 46 | 99.95 99 99.7 99.9 99.95 | 47.19 53.55 53.55 > 55.11 | 74.60 " No FIT | 55.11 | 23.30 | 2.03 2.3 2.30 > 2.3 | |
| 47 | 99 99.7 99.9 99.9 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | No FIT | 19.06 | 4.76 | 2.51 3.4 3.48 > 4.0 | 8 - 4.00 |
| 48 | 99 99.7 99.9 99.95 | 21.83 24.56 24.56 > 25.28 | NO FIT | 25.28 | 10.20 | 2.14 2.4 2.41 2.4 | |
| 50 | 99 99.7 99.9 99.95 | 10.69 > 17.05 17.05 > 17.05 | 9.59 LN 12.20 " 14.91 " 16.44 | 17.05 | 2.98 | 3.59 > 5.7 5.72 > 5.7 | |
| 52 | 99 99.7 99.9 99.95 | 16.69 18.12 17.03 > 18.12 | NO FIT | 18.12 | 5.64 | 2.96 3.2 3.02 > 3.2 | |
| 53 | 99 99.7 99.9 99.95 | 1.80 2.19 2.19 > 2.98 | NO FIT | 2.98 | 0.49 | 3.67 4.4 4.47 > 6.0 | |
| 54 | 99 99.7 99.9 99.95 | 9.70 9.78 9.78 > 10.98 | 9.50 SLN 12.38 " 15.43 " 17.18 " | 10.98 | 3.01 | 3.22 3.2 3.25 > 3.6 | |
| 55 | 99 99.7 99.9 99.95 | 0.69 0.77 0.77 > 0.84 | NO FIT | 0.84 | 0.26 | 2.65 2.9 2.96 > 3.2 | |
| 58 | 99 99.7 99.9 99.95 | 0.63 0.77 0.77 > 0.84 | 0.74 SLN 0.88 " 1.02 " 1.10 " | 0.84 | 0.24 | 2.63 3.2 3.21 > 3.5 | |
| 59 | 99 99.7 99.9 99.95 | 15.45 18.92 18.92 >19.78 | 11.34 LN 12.91 " 14.38 " 15.16 " | 19.78 | 5.81 | 2.67 3.2 3.26 > 3.4 | |
| 60 | 99 99.7 99.9 99.95 | 0.75 1.02 1.02 >1.03 | No FIT | 1.03 | 0.26 | 2.88 3.9 3.92 > 3.9 | |
| 61 | 99 99.7 99.9 99.95 | 21.41 24.64 24.64 >26.45 | NO FIT | 26.45 | 4.64 | 4.61 5.1 5.31 >5.7 | |
| 69 | 99 99.7 99.9 99.95 | 0.13 >0.14 0.14 >0.14 | NO FIT | 0.14 | 0.04 | 3.25 >3.5 3.50 >3.5 | |

(Cont'd)

| Mill No. | t - Tile | Non Parametric Estimate at 50% TL 5% TL | Distrib. Function Estimate Value Rasis | Max. Daily Value | Long Term Avg. | Variability 50% TL 5% TI | -Based | |
|-------------|-----------------------------|---|--|------------------------|----------------------|--|--------|------|
| 74 | 99 99.7 99.9 99.95 | 1.11 1.14 1.12 >1.14 | 1.29 LN 1.65 " 2.04 " 2.26 " | 1.14 | 0.38 | 2.92 3.00 2.95 >3.00 | | 3.00 |
| 78 | 99 99.7 99.9 99.95 | 5.60 5.96 5.96 >6.00 | 6.64 SLN 7.49 " 8.27 " 8.68 " | 6.00 | 2.46 | 2.28 2.42 2.42 > 2.44 | | 2.44 |
| 81 | 99 99.7 99.9 99.95 | 5.60 5.96 5.96 >6.00 | 6.27 LN 7.40 " 8.48 " 9.06 " | 6.00 | 2.72 | 2.05 2.19 2.19 > 2.23 | | 2.19 |
| 82 | 99 99.7 99.9 99.95 | 2.15 2.79 2.79 > 3.91 | NO FIT | 3.91 | 0.83 | 2.59 3.30 3.36 > 4.7 | | 4.71 |
| 83 | 99 99.7 99.9 99.95 | 0.086 > 0.092 0.092 > 0.092 | NO FIT | 0.092 | 0.03 | 2.86 > 3.0 [°] 3.07 > 3.0 [°] | | 3.07 |

NOTE: 1) Variability is the ratio of the indicated value to the long term average.

| | | TABLE | A7 | _INDUST | E OF VARI RY BIOLOG AXIMUM DA | ICALLY T | | EFFLUE | | |
|--------------------|-----------------------------|-----------------------------------|--------------------------|----------------------------------|--------------------------------------|------------------------|----------------------|-------------------|---------------------|--|
| Mill <u>No.</u> | % - <u>Tile</u> | Non Param Estimate 50% TL 5 | at | | 5. Function <u>imate</u> Basis | Max. Daily Value | Long Term Avg. | Variabi 50% TL | lity Bas 5% TL D | |
| 1 | 99 99.7 99.9 | | 91.5 09.1 - | No | FIT | 609.1 | 54.3 | 3.47 7.21 | 7.21 >11.2 | |
| | 99.95 | - | | | | | | - | - | |
| 2-1 | 99 99.7 99.9 99.95 | | 43.58 43.74 - - | 41.96 48.27 54.26 57.43 | SLN # # | 43.74 | 13.69 | 2.59 3.18 _ | 3.18 >3.20 _ | |
| 2-2 | 99 99.7 99.9 99.95 | | 35.22 | 38.17 49.78 62.11 69.16 | LN # # | 44.74 | 10.55 | 3.04 3.24 | 3.34 >4.24 - | |

| 8 - | Estima | ate at | | timate | Daily | Term | Variabi | lity Bas | sed U | |
|-------------|--------|--------|-------|--------|--------------|-------------|---------|----------|-------------|---------------|
| <u>Tile</u> | 50% TL | 58 TL | Value | Basis | <u>Value</u> | <u>Avg.</u> | 50% TL | 5% TL 1 | <u>.</u> F. | <u>M.D.V.</u> |
| 99 | 188.4 | 391.5 | No | FIT | 609.1 | 54.3 | 3.47 | 7.21 | | 11.2 |
| 99.7 | 391.5 | >609.1 | | | | | 7.21 | >11.2 | - | |
| 99.9 | - | - | | | | | - | - | - | |
| 99,95 | - | - | | | | | - | - | - | |

| 2-1 | 99 99.7 99.9 99.95 | 35.43 43.58 _ | 43.58 >43.74 _ _ | 41.96 48.27 54.26 57.43 | SLN " " | 43.74 | 13.69 | 2.59 3.18 - | 3.18 3.07 >3.20 3.53 - 3.96 - 4.20 | 3.20 |
|---------|-----------------------------|--------------------------|---------------------------|----------------------------------|---------------|-------|-------|------------------------|---|-------|
| 2-2 | 99 99.7 99.9 99.95 | 32.09 35.22 _ | 35.22 >44.74 _ | 38.17 49.78 62.11 69.16 | LN " " | 44.74 | 10.55 | 3.04 3.24 | 3.34 3.62 >4.24 4.72 - 5.89 - 6.56 | 4.24 |
| 2-3 | 99 99.7 99.9 99.95 | 25.33 36.34 _ | 36.34 >40.35 _ | 37.65 41.71 45.42 47.34 | SLN " " | 40.35 | 12.59 | 2.01 2.89 | 2.89 2.99 >3.20 3.31 - 3.61 - 3.76 | 3.20 |
| 2-4 | 99 99.7 99.9 99.95 | 32.35 34.48 - - | 34.48 >36.77 _ _ | 43.09 46.77 50.07 1.76 | SLN n n | 36.77 | 14.77 | 2.19 2.33 | 2.33 2.92 >2.49 3.17 - 3.39 - 3.50 | 2.49 |
| 2-5 | 99 99.7 99.9 99.95 | 38.49 53.82 _ _ | 53.82 >53.82 _ _ | 41.60 48.82 55.80 59.54 | SLN M | 53.82 | 15.82 | 2.43 3.40 - | 3.40 2.63 >3.40 3.09 - 3.53 - 3.76 | 3.40 |
| 2/(1-5) | 99 99.7 99.9 99.95 | 34.20 43.74 45.54 | 36.34 45.54 >53.82 | No | FIT | 53.82 | 13.48 | 2.53 3.24 3.38 | 2.69 - 3.38 - >3.99 - | 3.99 |
| 3-1 | 99 99.7 99.9 99.95 | 149.2 241.8 - | 241.8 >295.0 _ | 143.8 178.2 213.1 232.4 | LN " " | 295.0 | 50.21 | 2.97 4.82 - | 4.82 2.86 >5.88 3.55 - 4.24 - 4.63 | 5.88 |
| 3-2 | 99 99.7 99.9 99.95 | 217.8 391.6 - | 391.6 >608.4 _ | No | FIT | 608.4 | 55.03 | 3.95 7.12 - | 7.12 - >11.06 - | 11.06 |
| 3/(1-2) | 99 99.7 99.9 99.95 | 188.6 343.3 608.4 | 295.0 >608.0 >608.4 | 159.1 199.9 241.8 265.3 | LN " | 608.4 | 52.81 | 3.57 6.50 11.5 | 5.59 3.01 >11.5 3.78 >11.5 4.58 - 5.02 | 11.5 |
| 4 | 99 99.7 99.9 99.95 | 16.26 16.88 - | >16.88 >16.88 - | 20.93 26.11 31.40 34.35 | SLN " | 16.88 | 5.171 | 3.14 3.26 _ | >3.26 4.04 >3.26 5.05 - 6.07 - 6.64 | 3.26 |
| 5 | 99 99.7 99.9 99.95 | 8.06 8.23 - - | 8.23 >9.50 _ | No | FIT | 9.50 | 3.83 | 2.10 2.15 - | 2.15 - >2.48 - | 2.48 |
| 6 | 99 99.7 99.9 99.95 | 57.05 57.08 - | 57.08 >71.31 _ _ | No | FIT | 71.31 | 25.15 | 2.27 2.27 - - | 2.27 - >2.84 - | 2.84 |

TABLE A7 ESTIMATE OF VARIABILITY IN PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED EFFLUENTS MAXIMUM DAY - TSS (KLBS/DAY) (Cont'd)

| L1 | % - Tile | Non Par Estima 50% TL | | | Function imate Basis | Max. Daily Value | Long Term Avg. | Variabi 50% TL | lity Based U | pon M.D.V. |
|----|-----------------------------|-----------------------------|----------------------------|----------------------------------|----------------------------|------------------------|----------------------|------------------------|--|---------------|
| | 99 99.7 99.9 99.95 | 41.82 43.91 - - | 43.91 > 45.47 _ _ | No | FIT | 45.47 | 21.05 | 1.99 2.09 - | 2.09 - >2.16 - | 2.16 |
| | 99 99.7 99.9 99.95 | 12.93 18.51 _ _ | 18.51 >18.51 _ _ | 14.09 17.38 20.64 22.52 | SLN " " | 18.51 | 4.05 | 3.19 4.57 _ | 4.57 3.48 >4.57 4.29 - 5.10 - 5.56 | 4.57 |
| | 99 99.7 99.9 99.95 | 93.16 104.5 | 104.5 > 157.3 - | No | FIT | 157.3 | 10.84 | 8.59 9.64 _ _ | 9.64 - >14.5 - | 14.50 |
| | 99 99.7 99.9 99.95 | 17.16 17.89 _ _ | 17.89 >19.49 _ _ | 16.36 17.87 19.13 19.74 | N n # | 19.49 | 7.98 | 2.15 2.24 _ _ | 2.24 2.05 >2.44 2.24 - 2.40 - 2.47 | 2.44 |
| | 99 99.7 99.9 99.95 | 13.06 18.68 - | 21.47 > 21.47 | No | FIT | 21.47 | 6.35 | 2.06 2.94 _ | 3.38 - >3.38 - | 3.38 |
| | 99 99.7 99.9 99.95 | 18.35 18.97 _ | 18.97 >21.20 - - | 26.64 29.43 31.98 33.30 | SLN " | 21.20 | 8.16 | 2.25 2.32 | 2.32 3.26 >2.60 3.61 - 3.92 - 4.08 | 2.60 |
| | 99 99.7 99.9 99.95 | 7.11 7.96 _ | > 7.96 > 7.96 _ _ | 7.93 9.45 10.94 11.75 | SLN " " | 7.96 | 2.58 | 2.76 3.09 _ | 3.09 3.07 >3.09 3.66 - 4.24 - 4.55 | 3.09 |
| | 99 99.7 99.9 99.95 | 20.94 21.37 _ | > 21.37 > 21.37 | 19.85 23.74 27.56 29.63 | SLN " " | 21.37 | 6.52 | | > 3.28 3.04 > 3.28 3.64 - 4.22 - 4.54 | 3.28 |
| | 99 99.7 99.9 99.95 | 10.40 13.49 _ | 13.49 >14.87 _ | 8.56 10.98 13.49 14.92 | LN " | 14.87 | 2.60 | 4.00 5.18 - | 5.18 3.29 >5.72 4.22 - 5.19 - 5.74 | 5.72 |
| | 99 99.7 99.9 99.95 | 21.99 24.28 - - | 24.28 >27.79 _ | No | FIT | 27.79 | 6.36 | 3.45 3.82 - | 3.82 - >4.37 - | 4.37 |
| | 99 99.7 99.9 99.95 | 5.11 5.87 _ | 5.87 >6.34 _ _ | 7.40 8.18 8.89 9.27 | SLN " " | 6.34 | 2.31 | 2.21 2.54 _ | | 2.74 |
| A | 99 99.7 99.9 99.95 | 43.23 51.13 _ | 52.29 >52.29 _ | 40.42 51.22 62.40 68.68 | LN " | 52 .29 | 12.70 | 3.38 4.00 _ | | 4.09 |
| B | 99 99.7 99.9 99.95 | 11.40 13.61 _ | 13.61 >13.66 _ | 13.51 15.72 17.84 18.97 | SLN " " | 13.66 | 4.40 | 2.59 3.09 _ | | 3.10 |
| | 99 99.7 99.9 | 53.67 55.90 | 55.90 >65.51 - | 78.76 88.73 98.00 | SLN " | 65.51 | 24.06 | 2.23 2.32 - | | 2.72 |

| Mill No. | % - Tile | Non Parametric <u>Estimate at</u> 50% TL <u>5% TL</u> | | b. Function timate Basis | Max. Daily Value | Long Term Avg. | <u>Variabi</u> 50% TL | lity Ba | | Don M.D.V. |
|---------------|-----------------------------|---|----------------------------------|--------------------------------|------------------------|----------------------|---------------------------|-------------------------------|------------------------------|---------------|
| 22 | 99 99.7 99.9 99.95 | 10.01 10.70 10.70 11.18 | 14.52 16.02 17.40 18.11 | SLN m m | 11.18 | 4.63 | 2.16 2.31 _ | | | 2.41 |
| 23 | 99 99.7 99.9 99.95 | 10.07 > 11.08 11.08 > 11.08 | 10.86 12.12 13.27 13.88 | LN m n | 11.08 | 6.12 | | | | 1.81 |
| 24-1 | 99 99.7 99.9 99.95 | 34.82 > 36.34 36.34 > 36.34 | 29.21 39.12 49.92 56.19 | SLN " " | 36.34 | 6.61 | | > 5.50 > 5.50 _ _ | | 5.50 |
| 2 4- 2 | 99 99.7 99.9 99.95 | 10.00 > 10.68 10.68 > 10.68 | 11.68 14.26 16.83 18.25 | | 10.68 | 4.31 | | > 2.48 > 2.48 _ _ | | 2.48 |
| 24- 3 | 99 99.7 99.9 99.95 | 11.01 > 13.99 13.99 > 13.99 | No | FIT | 13.99 | 4.15 | | > 3.37 > 3.37 _ _ | - | 3.37 |
| 24/(1-3) | 99 99.7 99.9 99.95 | 21.42 24.35 34.82 > 36 .34 36.34 > 36.34 | No | FIT | 36.34 | 4.99 | 4.99 6.98 7.28 - | 4.87 > 7.28 > 7.28 - | - - - | 7.28 |
| 25 | 99 99.7 99.9 99.95 | 1.97 3.05 3.05 > 3.05 | 2.86 3.98 5.24 5.99 | | 3.05 | 0.61 | 3.23 5.00 _ | 5.00 > 5.00 _ _ | | 5.00 |
| 26 | 99 99.7 99.9 99.95 | 6.01 6.97 6.97 > 7.04 | 6.12 6.72 7.26 7.54 | | 7.04 | 3.74 | 1.61 1.86 _ | 1.86 >1.88 _ _ | | 1.88 |
| 27 | 99 99.7 99.9 99.95 | 34.68 38.58 38.58 > 43.35 | No | FIT | 43.35 | 12.18 | 2.85 3.17 _ _ | 3.17 > 3.56 _ | - - - | 3.56 |
| 28 | 99 99.7 99.9 99.95 | 19.02 19.92 19.92 > 20.02 | No | FIT | 20.02 | 7.83 | 2.43 2.54 _ _ | 2.54 > 2.56 _ | | 2.56 |
| 29 | 99.7 99.9 99.95 | 9.21 > 9.41 9.41 > 9.41 | 10.32 11.75 13.09 13.79 | LN " " | 9.41 | 5.27 | | > 1.79 > 1.79 - - | | 1.79 |
| 30 | 99 99.7 99.9 99.95 | 33.91 39.77 39.77 > 46.80 | 33.32 42.34 51.70 56.96 | LN # :. | 46.80 | 10.42 | 3.25 3.82 - | 3.82 >4.49 _ | 3.20 4.06 4.96 5.47 | 4.49 |

| Mill No. | % - <u>Tile</u> | Non Parametric Estimate at 50% TL 5% TL | | 5. Function timate Basis | Max. Daily Value | Long Term Avg. | Variability Based Upon 50% TL 5% TL D.F. M.D.V. |
|-------------|-----------------------------|---|----------------------------------|--------------------------------|------------------------|----------------------|---|
| 31 | 99 99.7 99.9 99.95 | 10.56 ×11.53 11.53 ×11.53 | 10.67 11.63 12.34 12.71 | N " " | 11.53 | 5.61 | 1.88 2.06 1.90 2.06 2.06 > 2.06 2.07 - 2.20 - 2.27 |
| 32 | 99 99.7 99.9 99.95 | 6.21 7.29 6.29 7.29 | 8.03 9.18 10.27 10.84 | SLN " " | 7.29 | 2.42 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 33 | 99 99.7 99.9 99.95 | 19.77 21.26 21.26 > 21.97 | No | FIT | 21.97 | 8.74 | 2.26 2.43 - $2.512.43$ > 2.51 - |
| 34 | 99 99.7 99.9 99.95 | 27.89 32.81 32.81 > 33.64 | No | FIT | 33.64 | 14.91 | 1.87 2.20 - 2.26 2.20 > 2.26 |
| 35 | 99 99.7 99.9 99.95 | 9.58 10.62 10.62 > 11.10 | No | FIT | 11.10 | 3.58 | 2.67 2.97 - 3.10 2.97 > 3.10 - |
| 36 | 99 99.7 99.9 99.95 | 28.95 33.68 33.68 > 34.21 | No | FIT | 34.21 | 5.01 | 5.78 6.72 - 6.82 6.72 > 6.82 - |
| 37 | 99 99.7 99.9 99.95 | 3.26 3.54 3.54 > 3.74 | 4.26 4.77 5.24 5.49 | SLN n n | 3.74 | 1.55 | 2.10 2.27 2.75 2.41 2.28 > 2.41 3.08 3.38 3.54 |
| 38 | 99 99.7 99.9 99.95 | 4.82 5.12 5.12 > 5.52 | No | FIT . | 5.52 | 2.25 | 2.14 2.28 - $2.452.28$ > 2.45 |
| 39-1 | 99 99.7 99.9 99.95 | 8.46 10.17 10.17 > 10.57 | No | FIT | 10.57 | 3.04 | 2.78 3.35 - 3.48 3.35 > 3.48 - |
| 39-2 | 99 99.7 99.9 99.95 | 3.78 4.09 3.87 > 4.18 | No | FIT | 4.18 | 1.93 | 1.96 2.12 - $2.172.01$ > 2.17 |
| 39-3 | 99 99.7 99.9 99.95 | 5.88 6.63 6.63 > 6.91 | No | FIT | 6.91 | 1.94 | 3.03 3.42 - $3.563.42$ > 3.56 |
| 39/(1-3) | 99 99.7 99.9 99.95 | 7.96 8.42 9.58 10.57 10.57 > 10.57 | No | FIT | 10.57 | 2.29 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 40 | 99 99.7 99.9 99.95 | 16.16 > 16.81 16.81 > 16.81 | 19.49 23.37 27.19 29.27 | LN " " | 16.81 | 7.75 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 41 | 99 99.7 22.2 99.95 | 56.89 63.49 63.49 > 63.49 | No | FIT | 63.49 | 13.9 | 4.09 4.56 - 4.56 4.56 > 4.56 - |

| Mill <u>No.</u> | % − <u>Tile</u> | Non Parametric Estimate at 50% TL 5% TL | | b. Function timate Basis | Max. Daily Value | Long Term Avg. | Variability Based Upon 50% TL 5% TL D.F. M.D.V. |
|--------------------|-----------------------------|---|----------------------------------|--------------------------------|------------------------|----------------------|---|
| 42B | 99 99.7 99.9 99.95 | 2.89 3.15 3.05 > 3.15 | No | FIT | 3.15 | 0.85 | 3.40 3.71 - $3.713.59 > 3.71$ - |
| 43 | 99 99.7 99.9 99.95 | 66.01 68.35 68.35 > 73.20 | 78.89 87.90 96.21 100.5 | SLN # # | 73.20 | 28.84 | 2.29 2.37 2.74 2.54 2.37 > 2.54 3.05 3.34 3.48 |
| 44 | 99 99.7 99.9 99.95 | 36.53 39.59 39.59 > 44.29 | 51.02 56.76 62.03 64.77 | S LN " " | 44,29 | 16.31 | 2.24 2.43 3.13 2.72 2.43 > 2.72 3.48 3.80 3.97 |
| 45 | 99 99.7 99.9 99.95 | 246.7 ×251.3 251.3 ×251.3 | 303.5 355.1 404.7 431.4 | SLN T T | 251.3 | 89.25 | 2.76 > 2.82 3.40 2.82 2.82 > 2.82 3.98 4.53 4.83 |
| 46 | 99 99.7 99.9 99.95 | 36.53 39.59 39.59 > 44.29 | 51.24 57.38 63.05 66.01 | SLN " | 44.29 | 14.88 | 2.45 2.66 3.44 2.98 2.66 > 2.98 3.86 4.24 4.44 |
| 47 | 99 99.7 99.9 99.95 | 25.45 29.48 29.48 > 30.32 | 24.93 30.04 35.09 37.84 | | 30.32 | 9.78 | 2.60 3.01 2.54 3.10 3.01 > 3.10 3.07 3.59 3.87 |
| 48 | 99 99.7 99.9 99.95 | 12.25 13.15 13.15 > 13.97 | No | FIT | 13.97 | 5.57 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 50 | 99 99.7 99.9 99.95 | 9.56 11.33 11.33 > 11.51 | 7.78 9.44 10.85 11.74 | | 11.51 | 2.97 | 3.21 3.81 2.62 3.88 3.81 > 3.88 3.18 3.65 3.95 |
| 52 | 99 99.7 99.9 99.95 | 19.70 23.44 23.44 > 24.82 | 25.27 32.25 39.51 43.61 | | 24.82 | 7,61 | 2.59 3.08 3.32 3.26 3.08 > 3.26 4.24 5.19 5.73 |
| 53 | 99 99.7 99.9 99.95 | 4.39 5.41 5.41 > 5.42 | No | FIT | 5.42 | 1.37 | 3.20 3.95 - 3.96 3.95 > 3.96 - |
| 54 | 99 99.7 99.9 99.95 | 14.01 17.11 17.11 > 18.16 | No | FIT | 18.16 | 3.30 | 4.25 5.18 - 5.50 5.18 > 5.50 - |
| 55 | 99 99.7 99.9 99.95 | 0.65 0.66 0.66 > 0.84 | 0.76 0.93 1.11 1.21 | SLN " " | 0.84 | 0.21 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 58 | 99 99.7 99.9 99.95 | 0.41 0.45 0.45 > 0.45 | 0.59 0.66 0.72 0.75 | SLB N N | 0.45 | 0.17 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| 59 | 99 99.7 99.9 99.95 | 45.00 54.60 54.60 > 72.53 | No | FIT | 72.53 | 11.53 | 3.90 4.74 - $6.294.74 > 6.29$ |
| 60 | 99 99.7 99.9 99.95 | 1.04 1.23 1.23 > 1.28 | No | FIT | 1.28 | 0.37 | 2.81 3.32 - 3.46 3.32 > 3.46 - |

| 61 | 99 99.7 99.9 99.95 | 24.77 35.68 35.68 > 59.47 | No | FIT | 59.47 | 4.88 | 5.08 7.31 - 12 7.31 > 12.19 - | 2.19 |
|------------|-----------------------------|----------------------------------|---------------------------------|---------------|-------|------|---|------|
| 6 4 | 99 99.7 99.9 99.95 | 0.17 > 0.18 0.18 > 0.18 | No | FIT | 0.17 | C.06 | | .83 |
| 69 | 99 99.7 99.9 99.95 | 0.14 0.15 0.15 0.15 | No | FIT | 0.15 | 0.06 | 2.33 2.50 - 2 2.50 2.50 - | .50 |
| 73 | 99 99.7 99.9 99.95 | 1.82 2.02 1.99 > 2.02 | 1.24 1.71 2.24 2.55 | LN ** | 2.02 | 0.29 | 6.28 6.97 4.28 6 6.86 > 6.97 5.90 7.72 8.79 | .97 |
| 74 | 99 99.7 99.9 99.95 | 0.97 1.02 0.99 >1.02 | 1.47 2.04 2.67 3.05 | LN ** | 1.02 | 0.31 | | .29 |
| 78 | 99 99.7 99.9 99.95 | 8.41 8.62 8.62 > 8.63 | 9.74 11.97 14.21 15.45 | LN " " | 8.63 | 3.48 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | .48 |
| 81 | 99 99.7 99.9 99.95 | 4.92 5.20 5.20 > 5.37 | No | FIT | 5.37 | 2.67 | 1.84 1.95 - 2 1.95 > 2.01 - | .01 |
| 82 | 99 99.7 99.9 99.95 | 2.07 2.33 2.33 > 2.37 | 2.31 2.76 3.20 3.44 | LN " | 2.37 | 0.94 | 2.20 2.48 2.46 3 2.48 > 2.52 2.94 3.40 3.66 | .52 |
| 83 | 99 99.7 99.9 99.95 | 0.10 > 0.10 0.10 > 0.10 | 0.13 0.16 0.19 0.20 | SLN " | 0.10 | 0.04 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | .50 |
| 85 | 99 99.7 99.9 99.95 | 1.62 1.99 1.99 > 2.13 | 2.23 3.14 4.18 4.80 | LN # # | 2.13 | 0.46 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | .63 |
| 91 | 99 99.7 99.9 99.95 | 1.41 >1.78 1.78 >1.78 | 2.24 3.14 4.16 4.76 | ĽN " " | 1.78 | 0.46 | 3.07 > 3.87 4.87 3 3.87 > 3.87 6.83 9.04 10.35 | .87 |
| 94 | 99 99.7 99.9 99.95 | 0.61 0.69 0.69 > 0.69 | 0.88 1.25 1.69 1.95 | LN " | 0.69 | 0.17 | | .06 |
| 96 | 99 99.7 99.9 99.95 | 0.37 > 0.45 0.45 > 0.45 | 0.44 0.56 0.69 0.77 | SLN " " | 0.45 | 0.12 | | .75 |

.

Note: Variability is the ratio of the indicated value to the long term average.

| | | | | | | | | | | 76 0 | | | |
|-----------|-------------------------|----------------|-------------------------|------------------|--------|---------|------------------|----------|------------|---------------|--------|----------|------------|
| | Durad | | runch | ed | | x. Star | | 1 | Crunch | ed <u>TSS</u> | F | ix. Sta | rt. |
| Mill No. | Prod. Category | N ¹ | Data LN ² | SLN ³ | F1 | x. Wind | ow <u>SLN</u> | <u>N</u> | Data LN | SLN | F N | ix. Wind | dow SLN |
| 1 | BK-DISS. | - | y ⁴ | - | - | Y | Y | Y | - | - | Y | - | - |
| 2-1 | | Y | - | - | Y | - | | Y | - | - | Y | - | - |
| 2-2 | 10 TI | Y | - | - | - | - | | Y | Y | - | Y | - | - |
| 2-3 | н н | Y | - | - | Y | Y | - | Y | - | - | Y | - | - |
| 2-4 | м н | Y | - | - | Y | - | - | Y | - | | Y | - | - |
| 2-5 | M N | Y | - | - | Y | - | - | Y | - | - | Y | - | - |
| 2/(1-5) | - | Y | - | ~ | Y | - | - | Y | - | - | Y | - | - |
| 3-1 | | Y | - | - | Y | - | - | Y | - | - | Y | - | - |
| 3-2 | * * | - | Y | - | - | Y | - | Y | - | - | Y | - | - |
| 3/(1-2) | ** n | _ | Y | _ | - | Y | _ | Y | _ | _ | ¥ | _ | _ |
| 4 | BK-MKT | Y | - | _ | Y | - | - | Y | _ | - | Y | - | _ |
| * 5 | BK AK <u>I</u> N A | . - | Y | | · _ | Y | - | Y | - | _ | Y | _ | - |
| 6 | H p | Y | - | _ | Y | | - | Y | _ | _ | Y | | _ |
| | DV- NVM | | | | | | | | | | | | |
| 7 8 | ВК-МКТ * * | Y | - | - | Y | ~ | - | Y Y | - | - | Y | - | - |
| o 9 | ** | Y | - | - | Y | - | - | r Y | - | - | - | - | - |
| 10 | BK-BCT | Y Y | - | - | Y Y | Y Y | - | r Y | - | - | - Y | Y | - |
| 10 | N N | I | - | - | | - | - Y | - | - | - | | - v | - |
| 11 | н н | - Y | - Y | ¥ - | - Y | - Y | 1 _ | | Y | - SS Data | Y | Y | - |
| 12 | 9 n | | I | - | Y | - | - | Y | | 55 Data | Y | Y | |
| 14 | n n | 1 | Y | - | Y | Y | - | r X | - Y | - | r Y | | - |
| 15 | er 11 | - Y | Y | - | r Y | Y | - | Y | r X | - Y | x _ | - | _ |
| 16 | BK-FINE | Y | - | _ | Y | - | _ | Y | Y | - | Y | Y | _ |
| 17 | вк- <u>г іме</u> п и | - | - | Y | - | Y | _ | - | - | | - | - | Y |
| 18 | м и | Y | Y | - | Y | Y | - | Y | Y | Υ. - | Y | Ŷ | - |
| 10 19A | | Y | Y | - | Y | Y | - | - | Y | _ | - | Y | _ |
| 19B | M 11 | Y | Y | | - | Ŷ | - | Y | Y | | Y | Y | _ |
| | | | | | | | | | | - | 1 | 1 | - |
| 20 | BK-FINE | Y | Y | - | Y | Y | - | | | SS Data | | | |
| 21 | M +1 | Y | - | - | Y | - | - | Y | - | - | Y | - | - |
| 22 | 11 11 | Y | Y | - | Y | Y | - | Y | Y | - | Y | Y | - |

TABLE A8ANALYSIS OF PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED
EFFLUENTS FOR SELECTED DISTRIBUTION FUNCTIONSTHIRTY CONSECUTIVE DAY EFFLUENT QUALITY (KLBS/DAY)

A-32

TABLE A8ANALYSIS OF PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED
EFFLUENTS FOR SELECTED DISTRIBUTION FUNCTIONS
THIRTY CONSECUTIVE DAY EFFLUENT QUALITY (KLBS/DAY)

| Mill No. | | rod. | C N ¹ | runche Dața LN ² | ed 🛛 | Fi | x. Sta x. Wind | dow | | Crunch Data | I | F F | ix. St ix. Wi | ndow |
|-------------|-------------|--------------|---------------------|-----------------------------------|------|----------|-------------------|-----|----------|----------------|------------|----------|------------------|------|
| MIII NO. | Late | egory | <u>N</u> | LN | SLN | <u>N</u> | LN | SLN | <u>N</u> | LN | SLN | <u>N</u> | LN | SLN |
| 23 | UBK- | -LNBD | Y | - | - | Y | Y | | Y | Y | - | Y | - | - |
| 24-1 | | n | Y | Y | - | Y | Y | - | Y | Y | - | - | Y | - |
| 24-2 | м | * | Y | - | - | Y | - | - | Y | Y | - | Y | - | - |
| 24-3 | н | H | Y | Y | - | Y | - | - | Y | - | - | - | Y | - |
| 24/(1-3) | n | | Y | Y | - | Y | Y | - | | Y | - | - | Y | - |
| 25 | Ħ | H | Y | Y | - | Y | Y | - | Y | Y | - | Y | - | - |
| 26 | M | н | Y | - | - | Y | - | - | Y | Y | - | Y | Y | - |
| 27 | | n | - | Y | - | - | Y | - | - | - | - | - | Y | - |
| 28 | | * | Y | - | - | ¥ | - | - | Y | Y | - | Y | Y | - |
| 29 | | H | Y | - | - | Y | - | - | Y | Y | - | Y | Y | - |
| 30 | N | | Y | Y | - | Y | ¥ | - | Y | Y | - | Y | Y | - |
| 31 | UBK | -CP | Y | - | - | Y | Y | - | Y | - | - | Y | - | - |
| 32 | M | M | - | - | Y | Y | Y | - | Y | - | - | Y | - | . – |
| 33 | | 11 | Y | - | - | Y | Y | - | Y | Y | - | - | Y | - |
| 34 | " | | Y | Y | - | Y | Y | - | Y | - | - | Y | - | - |
| 35 | UBK- PAP | -SPEC. | Y | - | - | Y | - | | Y | Y | _ | Y | - | - |
| 36 | SEM | I-CHEM | Y | Y | - | Y | Y | - | - | Y | - | - | Y | - |
| 37 | n | | Y | Y | - | Y | Y | - | Y | Y | - | Y. | Y | - |
| 38 | | | Y | Y | - | Y | Y | - | Y | Y | - | Y | - | - |
| 39-1 | M | | - | Y | - | - | Y | - | - | - | Y | - | Y | - |
| 39-2 | | | Y | - | - | Y | Y | - | Y | Y | - | Y | - | - |
| 39-3 | | | - | Y | - | - | - | Y | Y | Y | - | Y | Y | - |
| 39/(1-3) | | | - | Y | - | - | Y | - | - | Y | - | - | Y | - |
| 40 | UBK, | SEMI CHEM | Y | Y | - | Y | Y | - | Y | Y | - . | Y | Y | - |
| 41 | " | | - | Y | - | - | Y | - | Y | Y | - | Y | Y | - |
| 4 2B | * | " | - | Y | - | - | Y | - | - | Y | - | - | Y | - |
| 43 | м | • | Y | - | - | Y | Y | - | Y | Y | - | - | Y | - |
| 44 | SUL | F-DISS | Y | - | - | Y | Y | - | Y | Y | - | Y | Y | - |
| 45 | n | n | Y | - | - | Y | - | - | Y | - | - | Y | - | - |
| 46 | " | Ħ | Y | - | - | Y | Y | - | Y | Y | - | Y | Y | - |
| 47 | SUL | F-PAP | Y | - | - | Y | - | - | Y | - | - | Y | - | - |
| 48 | n | н | Y | - | - | Y | - | - | Y | Y | - | Y | Y | - |

TABLE A8

ANALYSIS OF PULP AND PAPER INDUSTRY BIOLOGICALLY TREATED <u>EFFLUENTS FOR SELECTED DISTRIBUTION FUNCTIONS</u> THIRTY CONSECUTIVE DAY EFFLUENT QUALITY (KLBS/DAY) (Cont'd)

| | | c | Crunch | eu | OD ₅ Fi | x. Sta: | rt | | Crunche | d <u>TS</u> | | ix. Sta | art. |
|----------|-------------------|------------|-------------------------|------------------|--------------------|---------------|------------|-------|------------|-------------|--------|---------------|-------------|
| Mill No. | Prod. Category | <u>N</u> 1 | Data LN ² | SLN ³ | Fi: N | x. Wind LN | dow SLN | N | Data LN | SLN | F N | ix. Wir LN | idow SLN |
| 50 | SULF-PAP | Y | - | - | Y | Y | _ | Y | Y | _ | Y | Y | |
| 52 | н н | - | _ | Y | - | - Y | - | Y | - | _ | Ŷ | Ŷ | _ |
| 53 | GNDWD-FINE | v | Y | - | Y | Y | _ | Y | Y | - | Y | Y | |
| 54 | и и | Y | Y | - | Y | Y | - - | Y | Y | _ | Y | Y | _ |
| 55 | INT-MISC. | Y | Y | _ | Y | Y | _ | Y | Y | _ | Y | Y | - |
| 58 | NI-MISC, | Y | Y | - | 1 _ | | - | | | - | - | _ | - |
| 59 | DEINK-TISS | _ | | - | | Y | | ¥ | Y | - | Y | Y | - |
| 60 | DEINK-T155 | r Y | Y | - | Ү | Y | - | Y | Y | - | Y | Y | - |
| | | - | - | - | Y | - | - | Y | - | - | Y | - | - |
| 61 | DEINK-FINE | | Y | - | - | Y | - | Y | Y | - | Y | Y | - |
| 64 | WSTPAP- TISS | | Limit | ted BOD | Data | | | Y | Y | - | Y | Y | · - |
| 69 | WSTPAP-BD | Y | Y | - | Y | Y | - | Y | Y | - | Y | Y | - |
| 73 | * * | | Limit | ted BOD | Data | | | - | - | Y | - | - | Y |
| 74 | | Y | Y | - | Y | Y | - | Y | Y | - | Y | - | - |
| 78 | NONINT- FINE | Y | - | - | Y | Y | _ ' | Y | Y | _ | Y | Y | - |
| 81 | | Y | Y | - | Y | Y | - | Y | Y | - | · _ | Y | - |
| 82 | | Y | - | - | Y | - | - | Y | Y | _ | Y | _ | _ |
| 83 | NONINT- | | | | | | | | | | | | |
| | TISS | | Limi | ited BO | D Data | | | Y | - | - | Y | - | - |
| 85 | n | | Lim: | ited BO | D Data | | | Y | Y | - | Y | Y | - |
| 91 | NONINT-BD | | Lim | ited BO | D Data | | | Y | Y | - | Y | Y | - |
| 94 | NONINT- MISC. | | Lim: | ited BO | D Data | | | Y | Y | - | - | Y | _ |
| 96 | | | Lim | ited BO | D Data | | | Y | - | • | Y | - | - |

Note: 1) N = Normal Distribution

2) LN = Log Normal Distribution

3) SLN = Shifted Log Normal Distribution

4) Y = Yes, Data adheres to Distribution Indicated at Top of Column

TABLE A9ESTIMATE OF VARIABILITY IN PULP AND PAPER INDUSTRY
BIOLOGICALLY TREATED EFFLUENTSTHIRTY CONSECUTIVE DAY EFFLUENT QUALITY - BOD (KLBS/DAY)

| Mill <u>No.</u> | Prod. Category | OBS. | | | Long Term Avg. | Est. (99th <u>Percen</u> (CD)(1 | n . | MA30CD Value | | ariability Based Upon F.S./F.W. | MA30CD |
|--------------------|-------------------|------|----|----|----------------------|---|-------|-----------------|------|---------------------------------------|--------|
| 1 | BK-DISS | 363 | 12 | 13 | 36.66 | 79.54 | 79.26 | 84.7 | 2.17 | 2.16 | 2.31 |
| 2-1 | | 352 | 11 | 12 | 8.95 | 13.60 | 13.74 | 13.59 | 1.52 | 1.54 | 1.52 |
| 2-2 | | 356 | 11 | 12 | 6.97 | 12.24 | 15.90 | 13.92 | 1.76 | 2.28 | 2.00 |
| 2-3 | M - M | 354 | 11 | 12 | 8.60 | 10.58 | 10.56 | 11.01 | 1.23 | 1.23 | 1.28 |
| 2-4 | # N | 355 | 11 | 12 | 9.03 | 12.21 | 11.97 | 11.04 | 1.35 | 1.33 | 1.23 |
| 2-5 | 01 M | 354 | 11 | 12 | 9.34 | 14.32 | 13.76 | 12.90 | 1.53 | 1.47 | 1.38 |
| 2/(1-5) | 47 BF | 1771 | 59 | 61 | 8.56 | 12.98 | 13.22 | 13.92 | 1.52 | 1.54 | 1.63 |
| 3-1 | n n | 300 | 10 | 11 | 27.26 | 48.55 | 45.67 | 44.80 | 1.78 | 1.67 | 1.64 |
| 3-2 | | 338 | 11 | 12 | 37.50 | 83.43 | 95.24 | 84.69 | 2.22 | 2.54 | 2.26 |
| 3/(1-2) | N 17 | 638 | 21 | 23 | 32.70 | 72.83 | 73.62 | 84.69 | 2.22 | 2.25 | 2,58 |
| 4 | вк-мкт | 178 | 5 | 8 | 3.56 | 5.58 | 5.78 | 7.61 | 1.57 | 1.62 | 2.14 |
| 5 | H H | 344 | 11 | 12 | 5.02 | 14.02 | 13.33 | 12.94 | 2.79 | 2.67 | 2.58 |
| 6 | N N | 361 | 12 | 12 | 14.20 | 21.58 | 21.79 | 19.80 | 1.52 | 1.53 | 1.39 |
| 7 | | 322 | 10 | 11 | 7.28 | 14.46 | 14.79 | 13.50 | 1.99 | 2.03 | 1.85 |
| 8 | | 277 | 9 | 11 | 3.52 | 6.11 | 6.41 | 6.77 | 1.74 | 1.82 | 1.92 |
| 9 | M M | 337 | 11 | 12 | 3.29 | 5.80 | 5.79 | 6.15 | 1.76 | 1.76 | 1.87 |
| 10 | BK-BLT | 385 | 12 | 13 | 6.04 | 9.65 | 9.86 | 10.03 | 1.60 | 1.63 | 1.66 |
| 11 | n n | 368 | 12 | 13 | 6.71 | 18,51 | 18.37 | 20.02 | 2.78 | 2.74 | 2,98 |
| 12 | n n | 341 | 11 | 13 | 5.31 | 9.89 | 10.14 | 9.51 | 1.86 | 1.91 | 1.79 |
| 13 | | 350 | 11 | 12 | 9.03 | 13.48 | 13.45 | 12.42 | 1.49 | 1.49 | 1.38 |
| 14 | 01 M | 255 | 8 | 11 | 1.65 | 3.37 | 3.20 | 2.94 | 2.04 | 1.94 | 1.78 |
| 15 | | 129 | 4 | 9 | 12.10 | - | 22.24 | 21.83 | - | 1.83 | 1.80 |
| 16 | BK-FINE | 376 | 12 | 13 | 0.99 | 1.38 | 1.34 | 1.39 | 1.39 | 1.35 | 1.40 |
| 17 | n n | 373 | 12 | 13 | 3.82 | 12.11 | 8.40 | 8.33 | 3.17 | 2.20 | 2.18 |
| 18 | ¥7 19 | 356 | 11 | 12 | 1.04 | 1.79 | 1.78 | 1.74 | 1.72 | 1.72 | 1.67 |
| 19A | n n | 145 | 4 | 9 | 2.58 | - | 3.91 | - | - | 1.52 | - |
| 19B | n n | 196 | 6 | 13 | 1.57 | 2.56 | 4.35 | 3.57 | 1.63 | 2.71 | 2.27 |
| 20 | N N | 265 | 8 | 9 | 3.27 | 5.65 | 5.46 | 5.52 | 1.73 | 1.67 | 1.69 |
| 21 | N 19 | 434 | 14 | 15 | 11.2 | 16.07 | 15.76 | 16.15 | 1.43 | 1.41 | 1.44 |
| 22 | M n | 242 | 8 | 12 | 5.31 | 8,70 | 9.29 | 9.21 | 1.64 | 1.75 | 1.73 |

.___

| TABLE A9 | ESTIMATE O | F VARIABILITY | IN PULE | AND | PAPER | INDUSTRY |
|----------|------------|---------------|---------|-------|-------|----------|
| |] | BIOLOGICALLY | TREATED | EFFLU | JENTS | |

THIRTY CONSECUTIVE DAY EFFLUENT QUALITY - BOD (KLBS/DAY) (Cont'd)

| Mill No. | Prod. Category | OBS. | No. of 30 Day OBS (CD)(FS/FW) | Long Term Avg. | Est. of 99th <u>Percentile (CD)(FS/FW</u>) | MA30CD Value | Variabili Based Up C.D. F.S./F.W | on |
|-------------|-------------------|------|--|----------------------|---|-----------------|--|------|
| 23 | UBK-LNBD | 175 | 5 12 | 2.92 | 4.75 5.20 | 5.15 | 1.63 1.78 | 1.76 |
| 24-1 | M () | 159 | 59 | 2.13 | 3.32 3.73 | 4.18 | 1.56 1.75 | 1.96 |
| 24-2 | * * | 164 | 5 12 | 3.04 | 4.96 5.54 | 5.59 | 1.63 1.82 | 1.84 |
| 24-3 | 68 ge | 177 | 5 13 | 2.39 | 3.57 3.83 | 3.59 | 1.49 1.60 | 1.50 |
| 24/(1-3) | R 90 | 500 | 16 32 | 2.52 | 4.61 4.83 | 5.59 | 1.83 1.92 | 2.22 |
| 25 | 92 pr | 292 | 9 11 | 0.80 | 1.71 1.69 | 1.47 | 2.14 2.11 | 1.84 |
| 26 | | 273 | 9 11 | 2.04 | 2.66 2.75 | 2.53 | 1.30 1.35 | 1.24 |
| 27 | 0¢ 79 | 333 | 11 12 | 4.86 | 10.26 10.19 | 9.87 | 2.11 2.01 | 2.03 |
| 28 | N 16 | 385 | 12 14 | 5.44 | 9.66 9.65 | 9.30 | 1.78 1.77 | 1.71 |
| 29 | | 166 | 5 11 | 3.09 | 4.35 4.52 | 7.17 | 1.41 1.46 | 2.32 |
| 30 | W # | 306 | 10 11 | 4.13 | 7.31 7.51 | 8.39 | 1.77 1.82 | 2.03 |
| 31 | UBK-CP | 218 | 7 12 | 4.31 | 7.28 7.68 | 7.57 | 1.68 1.78 | 1.77 |
| 32 | 14 M | 257 | 8 12 | 1.31 | 3.50 2.16 | 2.34 | 2.67 1.65 | 1.77 |
| 33 | | 315 | 10 15 | 5.16 | 7.98 7.91 | 7.80 | 1.55 1.53 | 1.51 |
| 34 | | 354 | 11 12 | 5.71 | 8.44 8.94 | 9.00 | 1.48 1.57 | 1.58 |
| 35 ' | UBK-SPEC PAP | 355 | 11 12 | 1.79 | 2.45 2.42 | 2,42 | 1.37 1.35 | 1.35 |
| 36 | SEMI-CHEM | 370 | 12 13 | 2.97 | 8.01 8.03 | 8.80 | 2.70 2.70 | 2.96 |
| 37 | • • | 362 | 12 13 | 1.85 | 4.35 4.05 | 5.02 | 2.35 2.19 | 2.71 |
| 38 | N N | 310 | 10 11 | 2.31 | 4.57 4.87 | 5.44 | 1.98 2.11 | 2.35 |
| 39-1 | N N | 333 | 11 11 | 0.89 | 3.79 3.87 | 2.47 | 4.26 4.35 | 2.78 |
| 39-2 | M 11 | 359 | 12 12 | 0.50 | 0.94 0.87 | 0.70 | 1.88 1.74 | 1.40 |
| 39-3 | 7 9 | 339 | 11 12 | 0.46 | 1.55 1.99 | 1.11 | 3.37 4.32 | 2.41 |
| 39/(1-3) |) ^N N | 1031 | 34 35 | 0.61 | 2.05 2.04 | 2.47 | 3.36 3.36 | 4.05 |
| 40 | UBK/SEMI- CHEM | 159 | 59 | 3.80 | 7.87 8.35 | 8.12 | 2.07 2.20 | 2.14 |
| 41 | м н | 347 | 11 13 | 8.06 | 16.99 17.24 | 16.97 | 2.11 2.14 | 2.11 |
| 42 | N N | 298 | 9 10 | 1.52 | 7.28 6.44 | 5.08 | 4.79 4.23 | 3.34 |
| 43 | т н | 347 | 11 12 | 19.9 | 27.54 26.91 | . 27.77 | 1.38 1.35 | 1.40 |
| 44 | SULF-DISS | 376 | 12 13 | 24.80 | 37.99 39.28 | 39.18 | 1.53 1.58 | 1.58 |
| 45 | n u | 221 | 78 | 20.50 | 25.40 25.25 | 24.26 | 1.24 1.23 | 1.18 |
| 46 | 17 PT | 422 | 14 14 | 23.30 | 35.26 35.61 | 37.80 | 1.51 1.53 | 1.62 |
| | | | | | | | | |

TABLE A9ESTIMATE OF VARIABILITY IN PULP AND PAPER INDUSTRY
BIOLOGICALLY TREATED EFFLUENTS
THIRTY CONSECUTIVE DAY EFFLUENT QUALITY - BOD (KLBS/DAY)
(Cont'd)

| Mill No. | Prod. Category | OBS. | | | Long Term Avg. | Est. of 99th <u>Percentile</u> (CD)(FS/FW) | MA30CD Value | | /ariability Based Upon <u>F.S./F.W.</u> | MA30CD |
|-------------|-------------------|------|----|----|----------------------|---|-----------------|------|---|--------|
| 47 | SULF-PAP | 421 | 14 | 14 | 4.76 | 7.13 7.08 | 7.65 | 1.50 | 1.49 | 1.61 |
| 48 | . М. М. | 370 | 12 | 13 | 10.2 | 17.58 17.08 | 16.21 | 1.72 | 1.67 | 1.60 |
| 50 | × + | 159 | 5 | 9 | 2.98 | 5.31 5.22 | 4.82 | 1.78 | 1.75 | 1.62 |
| 52 | • • | 244 | - | 12 | 5.64 | - 13.44 | 13.98 | - | 2.38 | 2.48 |
| 53 | GNDWD-FINE | 384 | 12 | 13 | 0.49 | 0.96 0.95 | 1.11 | 1.96 | 1.94 | 2.27 |
| 54 | 89 98 | 354 | 11 | 13 | 3.01 | 6.17 6.00 | 5.64 | 2.05 | 1.99 | 1.87 |
| 55 | INTMISC | 317 | 10 | 13 | 0.26 | 0.54 0.54 | 0.55 | 2.08 | 2.08 | 2.12 |
| 58 | ** ** | 381 | 12 | 13 | 0.24 | 0.48 0.50 | 0.51 | 2.00 | 2.08 | 2.13 |
| 59 | DEINK-TISS | 388 | 12 | 13 | 5.81 | 7.28 8.42 | 8.26 | 1.25 | 1.45 | 1.42 |
| 60 | | 369 | 12 | 13 | 0.26 | 0.53 0.52 | 0.48 | 2.04 | 2.00 | 1.85 |
| 61 | DEINK-FINE | 357 | 11 | 12 | 4.64 | 32.72 30.54 | 16.55 | 7.05 | 6.58 | 3.57 |
| 69 | WSTPAP-BD | 151 | 5 | 8 | 0.04 | 0.09 0.11 | 0.10 | 2.25 | 2.75 | 2.50 |
| 74 | * * | 283 | 9 | 11 | 0.38 | 0.73 0.80 | 0.73 | 1.92 | 2.11 | 1.92 |
| 78 | NON INT-FINE | 350 | 11 | 12 | 2.46 | 4.23 4.34 | 4.41 | 1.72 | 1.76 | 1.79 |
| 81 | н н | 382 | 12 | 13 | 2.72 | 4.48 4.80 | 4.38 | 1.65 | 1.76 | 1.61 |
| 82 | H H | 347 | 11 | 12 | 0.83 | 1.03 1.02 | 1.07 | 1.24 | 1.23 | 1.29 |
| 83 | NONINT-TISS | 144 | 4 | 10 | 0.03 | 0.06 0.06 | 0.07 | 2.00 | 2.00 | 2.33 |

NOTE: 1) Estimate equals: Long Term Average + 2.33 (Standard Deviation).

 MA30CD = Maximum Average for 30 Consecutive Days Derived from Data.

 Variability = The Ratio of the Thirty Day Values to the Long Term Average.

TABLE A10ESTIMATE OF VARIABILITY IN PULP AND PAPER INDUSTRY
BIOLOGICALLY TREATED EFFLUENTS

THIRTY CONSECUTIVE DAY EFFLUENT QUALITY - TSS (KLBS/DAY)

| Mill No. | Prod. Category | OBS. | | of Day IS | Long Term Avg. | Est, of 99th Percentile | MA30CD ² Value | с.р. | Variabili Based Op F.S./F.W. | ty ³ on <u>MA30CD</u> |
|------------------|-------------------|------|-------|-----------------|----------------------|--|------------------------------|------|------------------------------------|--|
| | | | (CD)(| FS/FW) | | $(\overline{CD})(\overline{FS}/\overline{FW})$ | | | | |
| 1 | BK-DISS | 374 | 12 | 13 | 54.3 | 96.85 96.80 | 104.5 | 1,78 | 1.78 | 1.92 |
| 2-1 | H H | 354 | 11 | 12 | 13.7 | 19.60 19.31 | 19.71 | 1.43 | 1.41 | 1.44 |
| 2-2 | n n | 356 | 11 | 12 | 10.5 | 17.17 18.40 | 19.56 | 1.64 | 1.75 | 1.86 |
| 2-3 | n n | 355 | 11 | 12 | 12.6 | 17.37 17.32 | 17.22 | 1.38 | 1.37 | 1,37 |
| 2-4 | ti ti | 356 | 11 | 12 | 14.8 | 19.73 19.37 | 19.76 | 1.33 | 1.31 | 1.34 |
| 2-5 | ** ** | 357 | 11 | 12 | 15.8 | 23.73 23.41 | 23.60 | 1.50 | 1.48 | 1.49 |
| 2/(1-5) | N N | 1778 | 59 | 61 | 13.5 | 20.83 21.03 | 23.60 | 1.54 | 1.56 | 1.75 |
| 3-1 | н н | 300 | 10 | 11 | 50.2 | 80.52 78.00 | 75.57 | 1.60 | 1.55 | 1,51 |
| 3-2 | H H | 350 | 11 | 12 | 55.0 | 89.16 96.29 | 104.5 | 1.62 | 1.75 | 1.90 |
| 3/(1-2) | n n | 650 | 21 | 23 | 52.8 | 84.73 93.54 | 104.5 | 1.60 | 1.77 | 1.98 |
| 4 | BK-MKT | 176 | 5 | 9 | 5.17 | 10.40 10.58 | 12.07 | 2.01 | 2.05 | 2.33 |
| 5 | H H | 356 | 11 | 13 | 3.83 | 5.19 5.40 | 5.74 | 1.36 | 1.41 | 1.50 |
| 6 | | 360 | 12 | 12 | 25.20 | 42.05 42.40 | 33.40 | 1.67 | 1.68 | 1.33 |
| 7 | M N | 328 | 10 | 11 | 21.00 | 36.74 38.04 | 30.90 | 1.75 | 1.81 | 1.47 |
| 8 | 10 N | 312 | 10 | 11 | 4.05 | 6.44 No Fit | 6.46 | 1.59 | - | 1.60 |
| 9 | M 11 | 337 | 11 | 12 | 10.80 | 29.40 35.26 | 33.40 | 1.67 | 1.68 | 1.33 |
| 10 | BK-BCT | 387 | 12 | 13 | 7.98 | 11.21 11.68 | 10.36 | 1.40 | 1.46 | 1.30 |
| 11 | ни | 373 | 12 | 13 | 6.35 | 12.05 10.40 | 10.20 | 1.89 | 1.64 | 1.61 |
| 13 | 67 H | 352 | 11 | 12 | 8.16 | 10.81 10.79 | 10.40 | 1.32 | 1.32 | 1.27 |
| 14 | n n | 141 | 4 | 10 | 2.58 | 4.83 5.17 | 4.38 | 1.87 | 2.00 | 1.70 |
| 15 | 11 TI | 129 | 4 | 9 | 6.52 | 9.96 11.84 | 12.62 | 1.53 | 1.82 | 1.94 |
| 16 | BK-FINE | 381 | 12 | 13 | 2.60 | 4.65 4.94 | 4.75 | 1.79 | 1.90 | 1.83 |
| 17 | M 11 | 379 | 12 | 13 | 6.36 | 33.28 30.01 | 18.04 | 5.23 | 4.72 | 2.84 |
| 18 | H H | 356 | 11 | 12 | 2.31 | 3.38 3.28 | 3.33 | 1.46 | 1.42 | 1.44 |
| 19A | H M | 273 | 9 | 12 | 12.8 | 26.42 26.88 | 28.97 | 2.06 | 2.10 | 2.26 |
| 19B | 11 TR | 417 | 13 | 16 | 4.40 | 8.32 7.73 | 8.04 | 1.89 | 1.76 | 1.83 |
| 21 | 11 I I | 446 | 14 | 15 | 24.10 | 40.96 40.20 | 34.59 | 1.70 | 1.67 | 1.44 |
| 22 | M M | 363 | 12 | 12 | 4.63 | 7.93 7.97 | 8.20 | 1.71 | 1.72 | 1.77 |
| 23 | UBK-LNBD | 172 | 5 | 12 | 6.12 | 7.35 8.21 | 7.73 | 1.20 | 1.34 | 1.26 |
| 24-1 | n n | 160 | 5 | 10 | 6.61 | 17.84 20.26 | 20.28 | 2.70 | 3.07 | 3.07 |
| 24-2 | 94 49 | 164 | 5 | 12 | 4.31 | 6.24 7.15 | 6.73 | 1.45 | 1.66 | 1.56 |
| 24-3 | 11 11 | 177 | 5 | 13 | 4.15 | 4.83 7.99 | 7.53 | 1.16 | 1.93 | 1.31 |
| 24/(1-3) | 87 04 | 501 | 16 | 33 | 4.99 | 11.73 13.32 | 20.28 | 2.35 | 2.67 | 4.06 |
| 25 | 17 17 | 286 | 9 | 11 | 0.61 | 1.26 1.30 | 1.19 | 2.07 | 2.13 | 1.95 |
| | | | | | | | | | | |

A-37

| | | Non Parametric | Distrib. Function | Max. | Long | | | | |
|--------------------|-----------------------------|--|--|----------------|--------------|------------------------|---|------------------------------|----------------|
| Mill <u>No.</u> | % - Tile | Estimate at 50% TL 5% TL | Estimate Value Basis | Daily Value | Term Avg. | Varia 50% TL | bility ¹ -F 5 <u>% TL</u> | Based D.F. | Upon M.D.V. |
| 10 | 99 99.7 99.9 99.95 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 16.75 SLN 18.98 " 21.07 " 22.17 " | 17.75 | 6.04 | 2.14 2.38 _ | 2.38 > 2.94 _ | 2.77 3.14 3.49 3.67 | 2.94 |
| 11 | 99 99.7 99.9 99.95 | 28.20 30.02 30.02 31.02 | No FIT | 31.02 | 6.71 | 4.20 4.47 _ _ | 4.47 > 4.62 _ | | 4.62 |
| 12 | 99 99.7 99.9 99.95 | 11.68 12.52 12.52 > 12.56 | 13.72 LN 16.58 " 19.41 " 20.95 " | 12.56 | 5,31 | 2.20 2.35 - - | 2.35 > 2.36 | 2.58 3.12 3.65 3.95 | 2.36 |
| 13 | 99 99.7 99.9 99.95 | 19.65 19.97 19.97 > 23.94 | 26.95 SLN 29.98 " 32.76 " 34.20 " | 23.94 | 9.03 | 2.18 2.21 - | 2.21 > 2.65 _ | 2.98 3.32 3.63 3.79 | 2.65 |
| 14 | 99 99.7 99.9 99.95 | 4.07 4.27 4.13 > 4.27 | No FIT | 4.27 | 1,65 | 2.47 2.50 - | 2.58 > 2.58 | - - - | 2.58 |
| 15 | 99 99.7 99.9 99.95 | 24.35 > 26.95 26.95 > 26.95 | 27.52 LN 32.34 " 37.01 " 39.51 " | 26.95 | 12.10 | 2.01 2.23 - - | > 2.23 > 2.23 - | 2.27 2.67 3.06 3.27 | 2.23 |
| 16 | 99 99.7 99.9 99.95 | 2.33 2.79 2.79 > 3.61 | NO FIT | 3.61 | 0.99 | 2.35 2.82 - - | 2.82 > 3.65 - | - - - | 3.65 |
| 17 | 99 99.7 99.9 99.95 | 9.88 12.73 12.73 > 13.16 | 11.69 SLN 15.19 " 18.90 " 21.06 " | 13.16 | 3.82 | 2.58 3.33 - | - | 3.06 3.98 4.95 5.51 | 3.45 |
| 18 | 99 99.7 99.9 99.95 | 2.70 2.79 2.79 > 2.82 | NO FIT | 2.82 | 1.04 | 2.60 2.68 - | 2.68 > 2.71 - - | - - - | 2.71 |
| 19A | 99 99.7 99.9 99.95 | 8.51 > 8.86 8.86 > 8.86 | NO FIT | 8.86 | 2.58 | 3.30 3.43 - | > 3.43 > 3.43 - - | - - - | 3.43 |
| 19B | 99 99.7 99.9 99.95 | 6.31 > 9.19 9.19 > 9.19 | 6.96 LN 9.59 " 12.53 " 14.27 " | 9.19 | 1.57 | 4.02 5.85 - | > 5.85 > 5.85 _ _ | | 5.85 |
| 20 | 99 99.7 99:95 | 17.44 34.29 34.29 > 34.29 = = | 14.59 SLN 21.18 " 28.88 " 33.58 " | 34.29 | 3.27 | 5.33 10.49 _ | 10.49 > 10.49 1 | | 10.49 |
| 21 | 99 99.7 99.9 99.95 | 19.63 22.02 22.02 > 22.46 | 19.88 N 21.45 " 22.76 " 23.39 " | 22.46 | 11.20 | 1.75 1.97 _ _ | | | 2.01 |
| 22 | 99 99.7 99.9 99.95 | 11.63 >12.73 11.90 12.73 | 15.84 SLN 17.57 " 19.16 " 19.97 " | 12.73 | 5.31 | 2.19 2.24 - - | | | 2.40 |

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TABLE A10ESTIMATE OF VARIABILITY IN PULP AND PAPER INDUSTRY
BIOLOGICALLY TREATED EFFLUENTSTHIRTY CONSECUTIVE DAY EFFLUENT QUALITY - TSS (KLBS/DAY)

A.

| (| C | on | it. | 'd |) |
|---|---|----|-----|----|---|
| | | | | | |

| Mill No. | Prod. Category | OBS. | 30 <u>O</u> I | . of Day BS FS/FW) | Long Term Avg. | | | MA30CD ² Value | Variabili Based Up <u>C.D. FS/FW</u> | ty ³ on <u>MA30CD</u> |
|-------------|-------------------|------|------------------|-----------------------------|----------------------|-------|--------|------------------------------|--|--|
| 59 | DEINK-TISS | 391 | 13 | 13 | 11.50 | 19.95 | 20.93 | 20.14 | 1.73 1.82 | 1.75 |
| 60 | м м | 369 | 12 | 13 | 0.37 | 0.65 | 0.65 | 0.57 | 1.76 1.76 | 1.54 |
| 61 | DEINK-FINE | 361 | 12 | 12 | 4.88 | 11.67 | 11.43 | 11.56 | 2.39 2.34 | 2.37 |
| 64 | WSTPAP-TISS | 192 | 6 | 10 | 0.06 | 0.14 | 0.13 | 0.13 | 2.33 2.17 | 2.17 |
| 69 | WSTPAP-BD | 151 | 5 | 8 | 0.06 | 0.12 | 0.13 | 0.11 | 2.00 2.17 | 1.83 |
| 73 | | 249 | 8 | 12 | 0.29 | 1.51 | 1.56 | 1.00 | 5.21 5.38 | 3.45 |
| 74 | N N | 293 | 9 | 11 | 0.31 | 0.52 | 0.56 | 0.49 | 1.68 1.81 | 1.58 |
| 78 | 19 (F | 350 | 11 | 12 | 3.48 | 6.49 | 6.47 | 5.97 | 1.86 1.86 | 1.72 |
| 81 | ** | 382 | 12 | 13 | 2.67 | 4.02 | 4.27 | 3.87 | 1.51 1.60 | 1.45 |
| 82 | ti pi | 348 | 11 | 12 | 0.94 | 1.28 | 1.31 | 1.27 | 1.36 1.39 | 1.35 |
| 83 | NONINT-TISS | 192 | 6 | 10 | 0.04 | 0.07 | 0.07 | 0.06 | 1.75 1.75 | 1.50 |
| 85 | | 336 | 11 | 12 | 0.46 | 1.03 | . 1.02 | 0.99 | 2.24 2.22 | 2.15 |
| 94 | NONINT-MISC | 271 | 9 | 13 | 0.17 | 0.31 | 0.34 | 0.32 | 1.82 2.00 | 1.88 |
| 96 | 41 H | 223 | 7 | 11 | 0.12 | 0.17 | 0.17 | 0.17 | 1.42 1.42 | 1.42 |

Note: 1) Estimate equals: Long Term Average + 2.33 (Standard Deviation)

 MA30CD - Maximum Average for 30 Consecutive Days Derived from Data

3) Variability: The Ratio of the Thirty Day Values to the Long Term Average

TABLE AllSUMMARY OF NCASI ANALYSIS OF
VARIABILITY FACTORS

| | Maximu Variabili | | Maximum 30 Consecutive Day Variability Factors | | |
|-------------------------------|---------------------|-------|---|---------------------|-------|
| Analysis Method | (BOD ₅) | (TSS) | Analysis Method | (BOD ₅) | (TSS) |
| NPA(99%, 50% TL) ¹ | 2.84 | 2.91 | Crunched Data | 1.98 | 1.91 |
| NPA(99.7%, 50% TL) | 3.35 | 3.42 | fs/fw ² | 1.98 | 1.98 |
| Observed Data | 3.61 | 3.83 | Observed Data | 1.91 | 1.82 |
| EPA(Prcposed)BCT | 3.00 | 3.00 | EPA(Proposed)BCT | 1.78 | 1.82 |

NOTE: 1) NPA(99%, 50% TL) = Non Parametric Analysis at the 99th Percentile With a 50% Tolerence Level

2) FS/FW = Fixed Start/Fixed Window Technique, See Text for Definition

TABLE A12MILLS ANALYZED FOR VARIABILITY EFFLUENTQUALITY COMPARED TO BPT LIMITATIONS(LBS/TON BASIS)

| | | ! | BOD ₅ | | TS | 55 | BOD | 5 <u>+ TSS</u> |
|--------------------------|------------------|--|---|------------------|-------------------|-----------------------------|-------------------------------|-----------------------|
| Prod. <u>Category</u> | <u>AA</u> (1) | $\frac{30CD + MD}{(2)}$ | <u>AA+30CD + MD</u> (3) | $\frac{AA}{(4)}$ | 10CD + MD (5) | AA+30CD+MD (6) | AA+30CD+MD (7) | <u>30CD+MD</u> (8) |
| BK-DISS. | | | | | | | 2-1, 2-2, 2-3, 2-4, 2-5 | |
| вк-мкт. | | | 9 | | | 5 | 4* | 6 |
| вк-вст | | | 12 | 12* | | 11 [*] , 13, 15 | 10, 14 | |
| BK-FINE | | | 19A | | | 22 | 16, 17, 18, 19B | |
| UBK-LNBD | | | | | -2, 24-3 3, 29 | | 23 [*] ,25 26 | |
| UBK-CP | | | | 31 | *, 32* | | | |
| UBK-SPEC. P | AP | | | No | one | | | |
| SEMI-CHEM. | | 39-1 | | | 37* | | 39-2, 39-3 | |
| UBK/SEMI | | | | | | | | 42-B |
| SULF-DISS. | | | | | | 44 [°] , 46 | | |
| SULF-PAP | | | | | | 48 | 47, 50 | |
| GRNWD-FINE | | | 54 | | | | 53* | |
| INT. MISC | | | Not App | plicable | 2 | | | |
| DEINK-TISS | | | 59* | 59* | | | 60* | |
| DEINK-FINE | | | | 61* | | | | |
| WSTPAP-TISS | 64 | | | | | 64 | | |
| WSTBAP-BD | | | | | 74 | | | 69* |
| NONINT-FINE | 82 | | | 81 | | 82 | 78* | 81 |
| NONINT-TISS | 5 | | | | | | 83* | |
| NONINT-BD | 91 | | | | | | | |
| NONINT-MISC | 2 | | Not App | licable | | | | |
| NOTES: | 30CD = | nnual (or Lo Maximum 30 aximum Day | ng Term) Avera Consecutive Day | ge y Avera | ge | | | |
| | Dev | | asterisk data ument Variabil Data Base. | | | | | |
| | Column | | hich meet the . limitations. | AA BOD | limitation | s but don't π | eet 30CD | |
| | Column | | which meet the | 30CD an | d MD limit | ations but do | not meet AA | |
| | Column | | which meet the et all three TS | | | | | 5 |
| | Column | | which meet the itations. | AA TSS | limitation | s but do not | meet 30CD and | 3 |
| | Column | | which meet the limitations fo | | d MD TSS 1 | imitations bu | it do not mee | t |
| | Column | for TS | which meet the 55 but do not m lumn 3. | | | | given | |
| | Column | 7: Mills TSS. | which meet all | three | limitation | s for both BC | D and | |

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| VARIATION IN H | EFFLUENT QUALITY | VARIABILITY |
|--------------------|------------------|----------------|
| AT SELECTED MI | LLS PROVIDING MU | JLTI YEAR DATA |

| 1111 10. | Ann. Avg. Perf. BOD TSS | | Maximum Day Variability Factors Based Upon | | | | | Maximum 30 Day Variability Factors Based Upon | | | |
|-------------|-------------------------------|-------|--|-------|---------------|-------|----------------------|---|-------|------------|--------------------|
| | | | 99%(50% TL) | | 99.7%(50% TL) | | Observed Max. Day | C.D. | | FS/FW | Observed MA30CD |
| | (#/T) | (#/T) | (BOD) | (TSS) | (BOD) | (TSS) | (BOD)(TSS) | (BOD) | (TSS) | (BOD)(TSS) | (BOD)(TSS) |
| -1 | 8.2 | 12.5 | 2.33 | 2.59 | 2.85 | 3.18 | 3.11 3.20 | 1.52 | 1.43 | 1.54 1.44 | 1.52 1.44 |
| -2 | 6.3 | 9.5 | 3.16 | 3.04 | 3.29 | 3.29 | 3.35 4.24 | 1.76 | 1.64 | 2.28 1.75 | 2.00 1.86 |
| 3 | 7.4 | 10.8 | 1.76 | 2.01 | 1.82 | 2.89 | 1.94 3.20 | 1.23 | 1.38 | 1.23 1.37 | 1.28 1.37 |
| -4 | 7.6 | 12.3 | 1.88 | 2.19 | 1.95 | 2.33 | 1.96 2.49 | 1.35 | 1.33 | 1.33 1.31 | 1.28 1.34 |
| -5 | 7.9 | 13.4 | 2.12 | 2.43 | 2.47 | 3.40 | 2.50 3.40 | 1.53 | 1.54 | 1.47 1.56 | 1.38 1.75 |
| 9-1 | 1.4 | 4.9 | 3.36 | 2.78 | 3.80 | 3.35 | 5.74 3.48 | 4.26 | _ | 4.35 3.62 | 2.78 2.39 |
| 9-2 | 0.8 | 3.0 | 2.56 | 1.96 | 2.86 | 2.01 | 2.94 2.17 | 1.88 | 1.55 | 1.74 1.55 | 1.40 1.63 |
| 9-3 | 0.7 | 3.0 | 3.11 | 3.03 | 3.26 | 3.43 | 3.41 3.56 | 3.37 | 2.20 | 4.32 2.16 | 2.41 1.95 |
| | | | | | | _ | _ | | | | |

OTE: 2-1, 2-2, etc. represent 1, 2, etc. years of performance at Mill No. 2.

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